

CROCO

Coastal and Regional Ocean COmmunity model

USGS within Croco

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OUTLINE

- * USGS model presentation
- * Recap on sediment model and features
 - * Bedload formulas
 - * Suspended load
 - * Bed model
- * Implementation of USGS within CROCO :
 - * Equations
 - * Code structure
 - * Parameters and input files
 - * Possible interfaces
 - * Waves forcing
 - * Bottom Boundary Layer
 - * Morphodynamics
- * Examples

USGS Sediment model :

- * Activated with the cppkey « #define SEDIMENT »
- * « legacy » model within CROCO
- * Native one, from the UCLA/ROMS Community / USGS also called as CSTMS model (package Community Sediment Transport Modeling System), Blaas et al. (2007), Warner et al. (2008) and Shafiei et al. (2021)
- * Originally included in ROMS-AGRIF, some divergences appears with CROCO version but there are some common development
- * Available in ROMS-RUTGERS and OAWST

USGS

- Recap on sediment model and features

BEDLOAD formulas

Bedload flux :

$$q_b = \Phi \sqrt{(s - 1)gd_{50}^3 \rho_s}$$

d_{50} : median size

ρ_s : grain density

τ_c : critical stress

$$s = \rho / \rho_s$$



⇒ Different parameterization available for the transport rate Φ

Adding Slope effect :

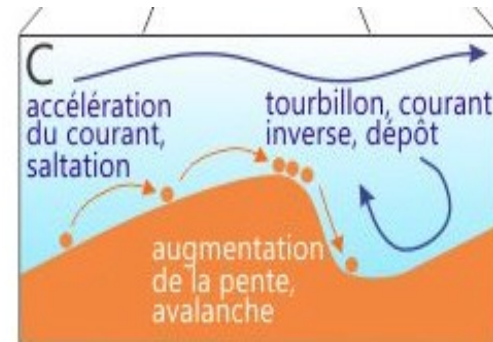
$$q_b = q_b \left(\frac{0.65}{(0.65 - \tan \beta) \cos \beta} \right) \quad \beta = \tan^{-1}(dz_b/dx)$$

cppkey

#define LESSER (by default)

Cppkey :

#define BEDLOAD



Bedload : Meyer-Peter Müller (MPM) formulation

Case of rivers, continental shelves etc :

Transport rate

(class dependent) :

$$\Phi = \max \left[8(\theta_s - \theta_c)^{1.5}, 0 \right]$$

$$\theta_s = \frac{\tau_s}{(s-1)gd_{50}} \quad \text{Shield parameter}$$

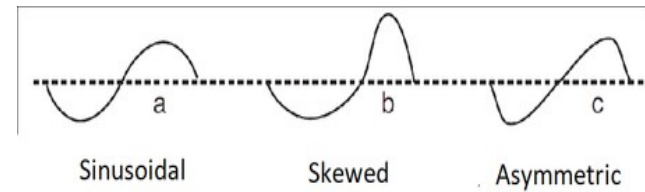
θ_c : critical Shield parameter (0,047)

τ_s : skin friction

Cppkey :

```
#define BEDLOAD_MPM
```

Bedload : Vander A formulation



Case of non-linear waves : asymmetric transport, lag effect ... :

- * Compute wave asymmetry effect
- * Shield parameter at half cycles
- * Evaluate phase lag

Transport rate

(class dependent) : crest + trough

$$\Phi = \frac{1}{T} \left[\frac{\theta_c}{|\theta_c|^{1/2}} T_c \left(\Omega_{cc} + \frac{T_c}{2T_{cu}} \Omega_{tc} \right) + \frac{\theta_t}{|\theta_t|^{1/2}} T_t \left(\Omega_{tt} + \frac{T_t}{2T_{tu}} \Omega_{ct} \right) \right],$$

$$\Omega_i = \mathcal{F}(\text{Shield } Cr) = \max \left(11 (|\theta_i| - \theta_{cr})^{1.2}, 0 \right),$$

Cppkey :

```
#define BEDLOAD_VANDERA
```

Suspended transport

For each sediment class grain (non cohesive) :

Suspended sediment transport

$$\frac{\partial C}{\partial t} + \frac{\partial U_i C}{\partial x_i} = \frac{\partial}{\partial x_i} \left(K_H \frac{\partial C}{\partial x_{1,2}} + K_V \frac{\partial C}{\partial x_3} \right) + \text{Sources / Sinks}$$

Erosion rate (E0) / Settling velocity (Ws) / critical shear stress for erosion are user defined

Erosion formulation

$$\text{Source} = E_0 (1 - \varphi) \frac{\tau_b - \tau_{ce}}{\tau_{ce}} \quad \text{when } \tau_b > \tau_{ce}$$

Bottom shear stress vs critical shear stress for erosion

If positive : material are added to the water column

Deposition formulation

$$\text{Sink} = w_s \frac{\partial C}{\partial z}$$

Settling velocity vs tracers gradient

Cppkey : #define SUSPLOAD

Cohesive bed module within USGS

Erodibility with Cohesive sediments:

- Sediments do not erode in the same way depending on whether they are cohesive or not
- Erodibility becomes a property of the bed layer and not only given for each sediment class
- **You have a critical shear stress for the erosion for each layer, which is increasing with depth and is time dependant**

$$\underbrace{\frac{\partial C}{\partial t}}_{\text{RATE}} = - \underbrace{\vec{\nabla} \cdot \vec{v} C}_{\text{ADVECTION}} + \underbrace{D_C}_{\text{MIXING}} - \underbrace{\frac{\partial w_s C}{\partial z}}_{\text{SETTLING}} + \underbrace{\frac{E}{\delta z_b}}_{\text{EROSION}} \Big|_{z=z_b}$$

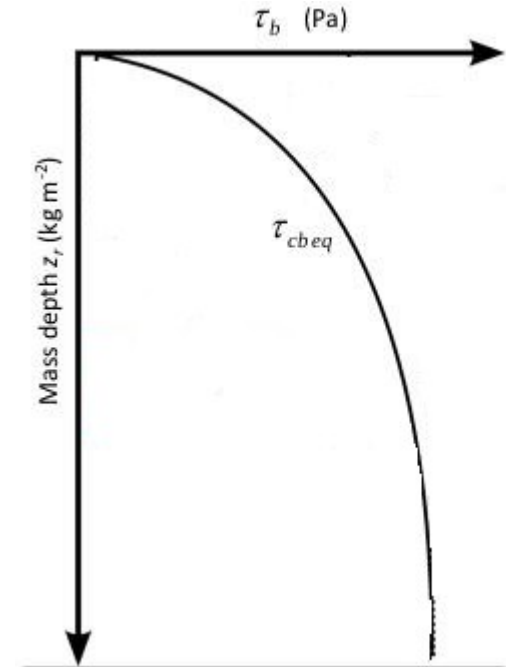
Initialization of the module:

- Initialization of the cohesive bed module on namelist sediment.in by user
 - * A global critical shear stress profile at equilibrium for erosion (τ_{cbeq})

$$\tau_{cbeq} = a \exp \left[\frac{\ln(z_p) - \text{offset}}{\text{slope}} \right]$$

- * Damping parameters to accelerate or not each process during runtime
 - * Timescale (s) T_c : for consolidation /
 - T_s : for swelling

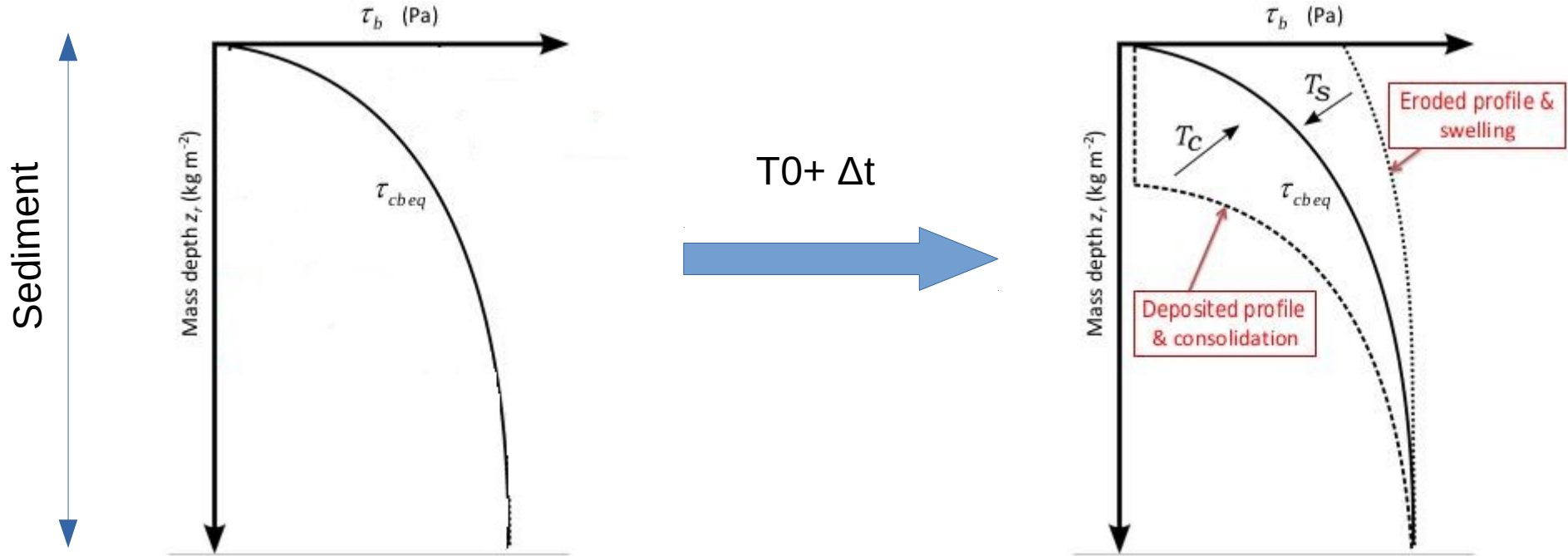
Shear stress z profile :



Runtime :

* some differences can occur between τ_{cbeq} and the critical shear stress for the erosion profile (τ_b) in each layer

* τ_b profile is varying in time and then will be nudged by the model over timescale T_c or T_s toward the equilibrium profile during this period

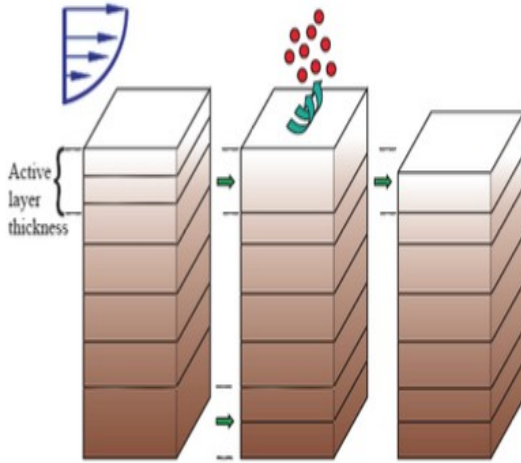


Cppkey : #define COHESIVE_BED / MIXED_BED

Bed model

Active layer thickness (Harris and Wiberg, 1997).

$$Z_a = k_1(\tau_w \cdot \tau_c) + k_2 D_{50}$$



Erosion. ($\tau_b > \tau_c$)

Mix sediment from lower layers so that surface layer is at least z_a thick. Split bottom layer. Erode from surface layer.

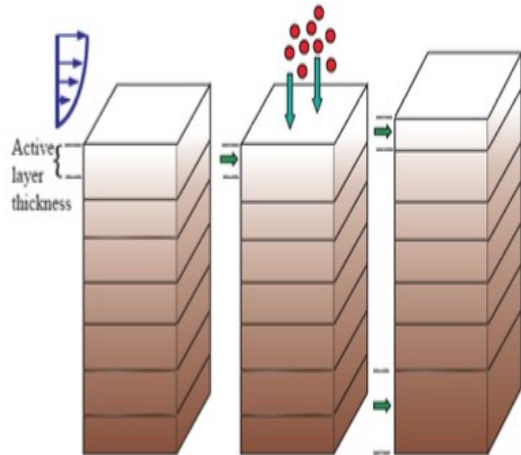
erosion_flux_i =

$$\text{MIN} \left[\begin{array}{l} dt \cdot E_i \cdot (1 - \text{poro}) \cdot \text{frac}_i \cdot (\tau_w / \tau_{c,i} \cdot 1) \\ \rho_i \cdot (1 - \text{poro}) \cdot \text{frac}_i \cdot z_a + \text{dep_flux}_i \end{array} \right]$$

Erosion

for $\tau_b > \tau_{ce}$

Number of layers is fixed



Deposition.

Rule: create new layer if deposition > 5 mm (user defined). Mix surface layer to be at least z_a thick. Combine bottom layer.

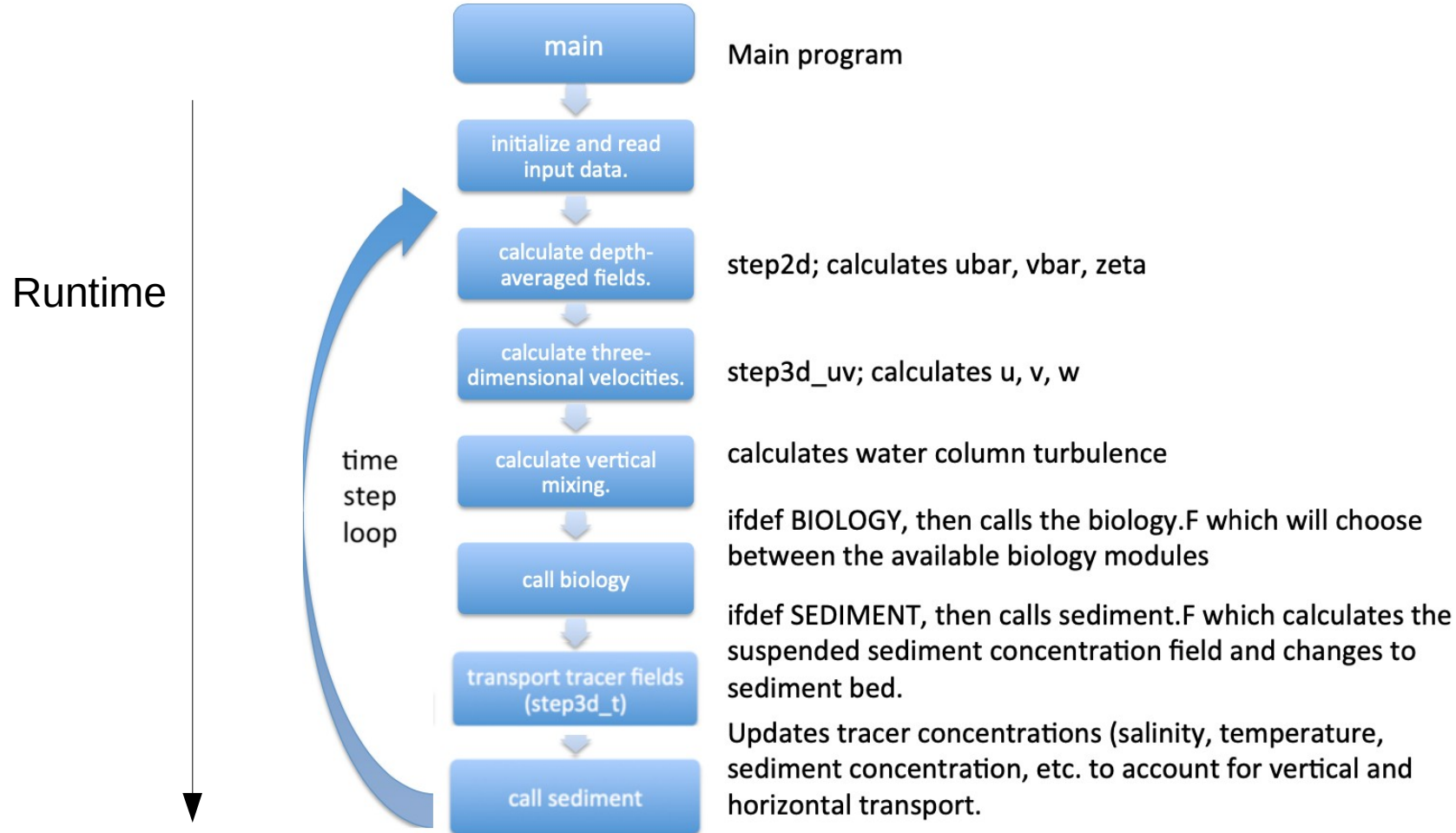
$$\frac{\partial C_i}{\partial t} = -w_{s,i} \frac{\partial C}{\partial z}$$

Deposition

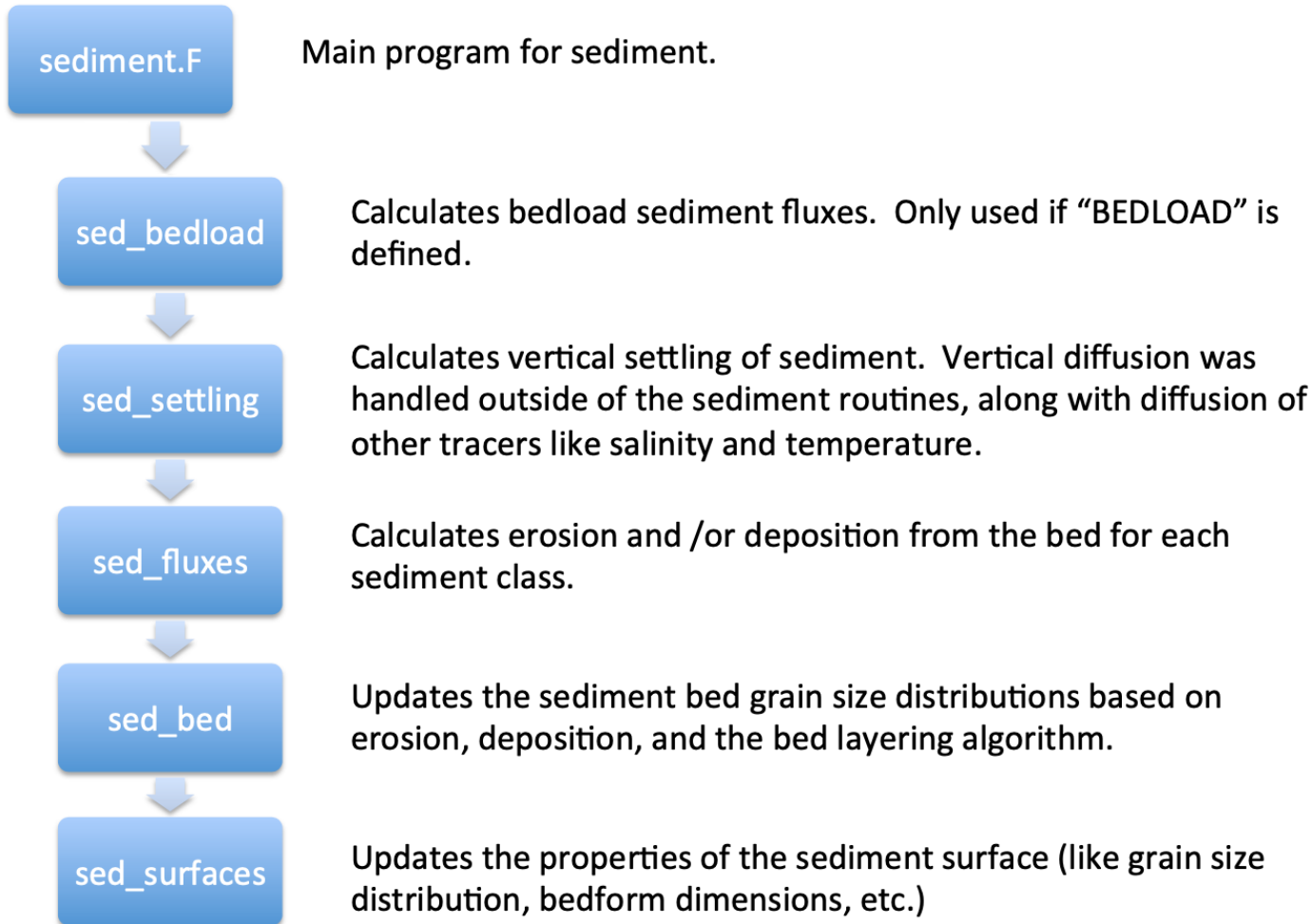
Rule: create a new layer for deposition if top layer > 1mm

Code structure

Code structure (1)



Code structure (2)



Code structure (3)

```
if defined NONLINEAR && defined SEDIMENT && defined BEDLOAD

-----

This routine computes sediment bedload transport using the Meyer-
Peter and Muller (1948) formulation for unidirectional flow and
Soulsby and Damgaard (2005) algorithm that accounts for combined
effect of currents and waves.

References:

Meyer-Peter, E. and R. Muller, 1948: Formulas for bedload transport
In: Report on the 2nd Meeting International Association Hydraulic
Research, Stockholm, Sweden, pp 39-64.

Soulsby, R.L. and J.S. Damgaard, 2005: Bedload sediment transport
in coastal waters, Coastal Engineering, 52 (8), 673-689.

Warner, J.C., C.R. Sherwood, R.P. Signell, C.K. Harris, and H.G.
Arango, 2008: Development of a three-dimensional, regional,
coupled wave, current, and sediment-transport model, Computers
& Geosciences, 34, 1284-1306.

-----
```

sed_bedload

1. Calculate correct bed stresses.
2. Calculate bedload transport rate using one of two relationships.
3. Accounts for bed slope.
4. Calculate bedload flux convergence and divergence that lead to erosion and deposition.
5. Limit erosion to amount of sediment available, and deposition to not shoaling.
6. Updates sediment bed properties.

Code structure (4)

```
#if defined NONLINEAR && defined SEDIMENT && defined SUSPLOAD

!-----!
! This routine computes the vertical settling (sinking) of suspended !
! sediment via a semi-Lagrangian advective flux algorithm. It uses a !
! parabolic, vertical reconstruction of the suspended sediment in !
! the water column with PPT/WENO constraints to avoid oscillations. !
!
! References: !
!
! Colella, P. and P. Woodward, 1984: The piecewise parabolic method !
! (PPM) for gas-dynamical simulations, J. Comp. Phys., 54, 174-201. !
!
! Liu, X.D., S. Osher, and T. Chan, 1994: Weighted essentially !
! nonoscillatory schemes, J. Comp. Phys., 115, 200-212. !
!
! Warner, J.C., C.R. Sherwood, R.P. Signell, C.K. Harris, and H.G. !
! Arango, 2008: Development of a three-dimensional, regional, !
! coupled wave, current, and sediment-transport model, Computers !
! & Geosciences, 34, 1284-1306. !
!-----!
```

sed_settling

1. Vertical settling of sediment.
2. Biology routine uses same scheme for particulate classes.
3. Updates concentration fields for vertical settling.
4. Also calculates flux of sediment into the bed.
5. Does the calculations separately for each sediment type.

Code structure (5)

```
#if defined NONLINEAR && defined SEDIMENT && defined SUSPLOAD
```

```
This computes sediment bed and water column exchanges: deposition,  
resuspension, and erosion.
```

References:

```
Warner, J.C., C.R. Sherwood, R.P. Signell, C.K. Harris, and H.G.  
Arango, 2008: Development of a three-dimensional, regional,  
coupled wave, current, and sediment-transport model, Computers  
& Geosciences, 34, 1284-1306.
```

sed_fluxes

1. Exchange of sediment between water column and seabed.
2. First – calculates bed stresses.
3. Calculates erosion based on

$$E_{s,m} = E_{0,m}(1 - \phi) \frac{\tau_{sf} - \tau_{ce,m}}{\tau_{ce,m}}, \quad \text{when } \tau_{sf} > \tau_{ce,m} \quad (23)$$

where E_s is the surface erosion mass flux ($\text{kg m}^{-2} \text{s}^{-1}$), E_0 is a bed erodibility constant ($\text{kg m}^{-2} \text{s}^{-1}$), ϕ is the porosity (volume of voids/total volume) of the top bed layer, and m is an index

4. Erosion limited to amount of each size class in the surface layer + whatever would have settled.
5. The net erosion for each sediment class is called “ero_flux”.
6. Updates water column concentration in bottom water layer for the erosion and deposition.

Code structure (6)

sed_bed

1. The longest sediment routine (800 lines).
2. Keeps track of sediment distributions and properties in bed layers.
3. Has net erosion for each sediment class as “ero_flux” from sed_fluxes.F.
4. Has amount settling to bed as “settling_flux” from sed_settling.F.
5. The net erosion for each sediment class is the difference of “ero_flux” and “settling_flux”.
 - a. If “ero_flux – settling_flux” < 0, then you have net deposition of this sediment class. Add sediment to the top layer. When the top layer gets thick, split off a new top layer.
 - b. If “ero_flux – settling_flux” > 0, then you have net erosion of this sediment class. Remove sediment from the top layers.
 - c. Adjust layers if you needed to add a complete layer or erode one.

```
#if defined NONLINEAR && defined SEDIMENT && !defined COHESIVE_BED

-----
This routine computes sediment bed layer stratigraphy.
-----
Warner, J.C., C.R. Sherwood, R.P. Signell, C.K. Harris, and H.G.
Arango, 2008: Development of a three-dimensional, regional,
coupled wave, current, and sediment-transport model, Computers
& Geosciences, 34, 1284-1306.
-----
```

Model options

Sediment parameters

- Hard coded
 - Number of layers
 - Number of sediment classes

=> in param.h

```
!
# ifdef SEDIMENT
! NSAND      Number of sand classes
! NMUD       Number of mud classes
! NGRAV      Number of gravel classes (not implemented...)
! NST        Number of sediment (tracer) size classes
! NLAY       Number of layers in sediment bed
!
      integer NSAND, NMUD, NGRAV, NST, NLAY
# ifdef DUNE
#   ifdef ANA_DUNE
      parameter (NSAND=1, NMUD=0, NGRAV=0)
      parameter (NLAY=11)
#   else
      parameter (NSAND=2, NMUD=0, NGRAV=0)
      parameter (NLAY=10)
#   endif
# elif defined SED_TOY
#   if defined SED_TOY_RESUSP || defined SED_TOY_CONSOLID
      parameter (NSAND=2, NMUD=2, NGRAV=0)
      parameter (NLAY=41)
#   elif defined SED_TOY_FLOC
      parameter (NSAND=4, NMUD=15, NGRAV=0)
      parameter (NLAY=20)
#   elif defined SED_TOY_ROUSE
      parameter (NSAND=0, NMUD=6, NGRAV=0)
      parameter (NLAY=1)
#   endif
# else
      parameter (NSAND=2, NMUD=0, NGRAV=0)
      parameter (NLAY=1)
# endif
      parameter (NST=NSAND+NMUD+NGRAV)
      parameter (ntrc_sed=NST)
# else
      parameter (ntrc_sed=0)
# endif /* SEDIMENT */
!
```

Model options

Sediment CPP keys

- Main keys :
 - SEDIMENT
 - SUSPLOAD
 - BEDLOAD

=> stick with default choices

Related CPP options:

SUSPLOAD	Activate suspended load transport
BEDLOAD	Activate bedload transport
MORPHODYN	Activate morphodynamics
BEDLOAD_VANDERA	van der A formulation for bedload (van der A et al., 2013)
BEDLOAD_MPM	Meyer-Peter-Muller formulation for bedload (Meyer-Peter and Muller, 1948)
SLOPE_LESSER	Lesser formulation for avalanching (Lesser et al, 2004)
SLOPE_NEMETH	Nemeth formulation for avalanching (Nemeth et al, 2006)
BEDLOAD_UP1	Bedload flux interpolation: upwind 1st order
BEDLOAD_UP5	Bedload flux interpolation: upwind 5th order
BEDLOAD_WENO5	Bedload flux interpolation: WENO 5th order
ANA_SEDIMENT	Set analytical sediment size, initial ripple and bed parameters
ANA_BPFLUX	Set kinematic bottom flux of sediment tracer (if different from 0)
SPONGE_SED	Gradually reduce erosion/deposition near open boundaries

Preselected options:

```
#ifdef SEDIMENT
# undef MUSTANG
# define ANA_SEDIMENT
# define SPONGE_SED
# define Z0_BL
# define Z0_RIP
# ifdef BEDLOAD
#   ifdef BEDLOAD_VANDERA /* default BEDLOAD scheme */
#   elif defined BEDLOAD_MPM
#   elif defined BEDLOAD_WULIN
#   elif defined BEDLOAD_MARIEU
#   else
#     if (defined WAVE_OFFLINE || defined WKB_WWAVE ||\
        defined ANA_WWAVE || defined OW_COUPLING)
#       define BEDLOAD_VANDERA
#     else
#       define BEDLOAD_MPM
#     endif
#   endif
# endif
```

Model options

Input file

- Dans croco.in :

```
sediments: input file
           sediment.in
sediment_history_fields: bed_thick bed_poros bed_fra(sand,silt)
                        20*F
```

- Additional file at run time : [sediment.in](#)

Consistent with param.h :

- Number of layers
- Number of sediment classes

```
1 Stitle (a80)
CROCO - Sediment - Test

2 Sd(1-NST), CSED, SRHO, WSED, ERATE, TAU_CE, TAU_CD, BED_FRAC(1:NLAY)
  0.125 9.9 2650. 9.4 25.0e-5 0.05 0.14 0.4 0.4
  0.050 0.0 2650. 1.6 4.0e-5 0.01 0.14 0.6 0.6

3 BTHK(1:NLAY)
  1. 10.

4 BPOR(1:NLAY)
  0.41 0.42

5 Hrip
  0.03

6 Lrip
  0.14

7 bedload_coeff
  0.

8 morph_fac
  10.

99 END of sediment input data
```

> **Sd** : Diameter of grain size class [mm].

> **CSED** : Initial concentration (spatially uniform) [kg/m³].

> **SRHO** : Density of sediment material of size class [kg/m³].

Quartz: SRHO=2650 kg/m³

> **WSED** : Settling velocity of size class [mm/s].

Typically (Soulsby, 1997):

$$WSED = 10^3 (visc (\sqrt{10.36^2 + 1.049D^3} - 10.36) / D_{50} \text{ [mm/s]})$$

$$\text{with } D = D_{50} (g (SRHO/\rho_0 - 1) / (visc^2))^{0.33333}$$

$$D_{50} = 10^{-3} Sd \text{ [m]}$$

$$visc = 1.3 \cdot 10^{-3} / \rho_0 \text{ [m}^2/\text{s]}$$

> **ERATE** : Erosion rate of size class [kg/m²/s].

Typically:

$$ERATE = 10^{-3} \gamma_0 WSED SRHO \text{ [kg/m}^2/\text{s]}$$

$$\text{with } \gamma_0 = 10^{-3} - 10^{-5} \text{ (Smith \& McLean, 1977)}$$

> **TAU_CE** : Critical shear stress for sediment motion [N/m²]

(initiation of bedload for coarses, suspension for fines). Typically : $TAU_{CE} = 6.4 \cdot 10^{-7} \rho_0 WSED^2$ [N/m²]

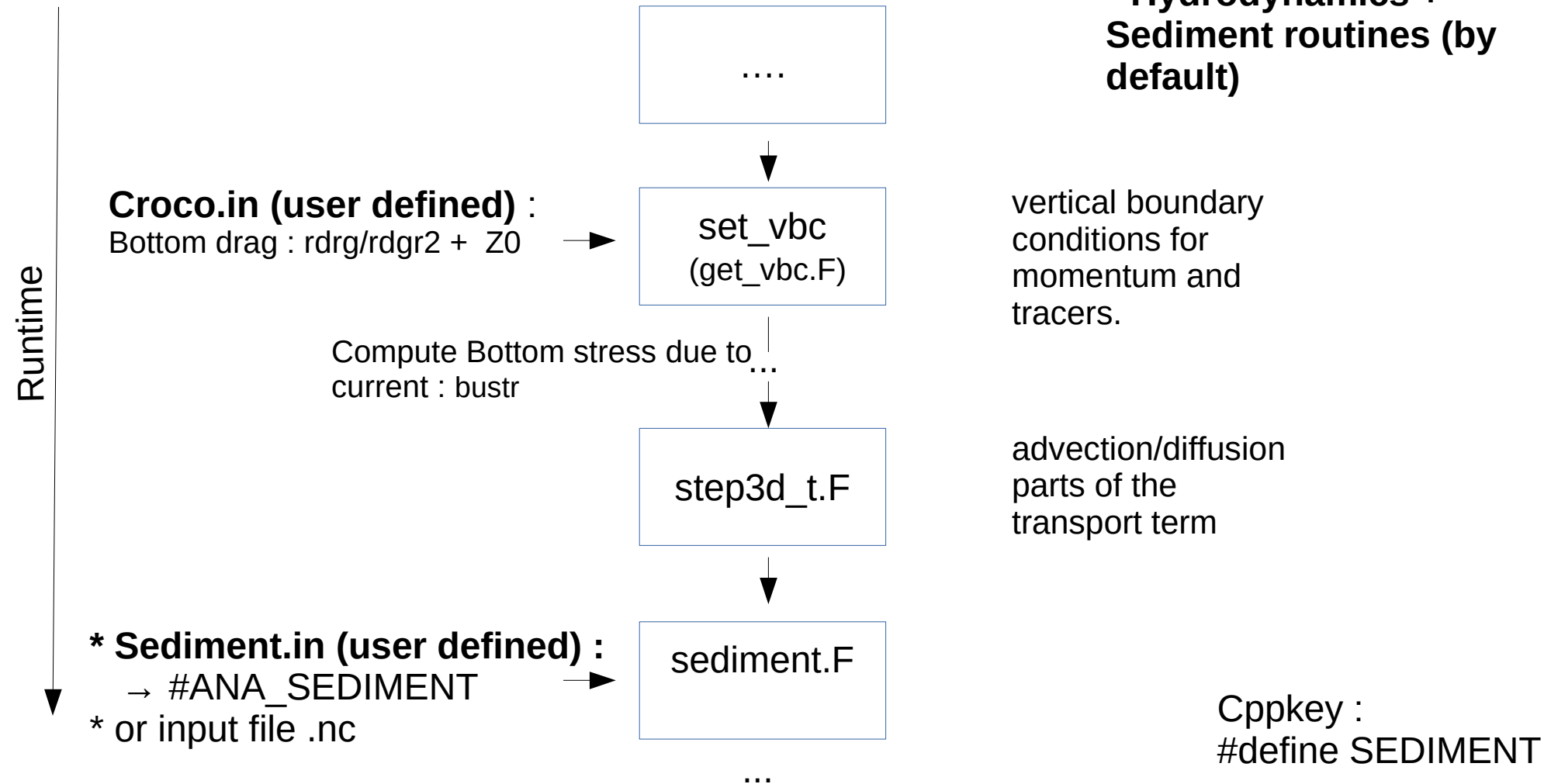
> **TAU_CD** : Critical shear stress for deposition of cohesive sediments [N/m²]

> **BED_FRAC** : Volume fraction of each size class in each bed layer (NLAY columns)

$$[0 < BED_FRAC < 1]$$

Possible interfacing

No Interfacing



Waves forcing overview

Description	Analytical Specified / constant value	Internal Wave Maker Waves resolving simulation (Non boussinesq / w solve explicetely)	Embedded wave model within Croco		Online data	Offline data
			WKB primary waves and empirical breaking model parameters with offshore wave amplitud/period boundary conditions		Spectral wave model (WW3..)	clim/reanalysis (ERA5...)
			Initialized by croco.in	boundary forcing from other wave data		
Advantages	Cheap	better resolved at the bottom / no use of wave average equation	Cheap / No waves generation / parametrizations for wave breaking and bottom drag		Realistic	
cppkey	#ANA_WWAVE	#WAVE_MAKER #NBQ	#WKB_WWAVE #ANA_BRY_WKB	#WKB_WWAVE	#OW_COUPLING	#WAVE_OFFLINE
routine	analytical.F	wave_maker*.h	wkb_wwave.F		get_wwave.F	
				get_bry_wkb.F		
Parameters	Hs,T,DD	Hs,T,DD...	Hs, T, DD + breaking parameters			
User def. file	Analytical.F	wave_maker*.h	Croco.in (wkb_wwave/wkb_roller)			

⇒ Estimate wave associated variables usually pass to wave current interaction (#MRL_WCI) (based on wave average equation, compute additional terms , stokes drift) and Bottom Boundary layer (#BBL) routines

Bottom boundary layer

Goal :

- * Variability of gradients in velocity and suspended-sediment concentrations near the bottom
- * Take account of the change of rugosity due to sediment in bottom stress computation
- * Parameterize the effect of surface waves on bottom stresses and apparent roughness

⇒ BBL formulation :

$$\bar{\tau}_{wc} = \tau_c \left(1 + 1.2 \left(\frac{\tau_w}{\tau_w + \tau_c} \right)^{3.2} \right)$$

- account for current stress at the bottom
- account for wave stress

$$\tau_c = \frac{\kappa^2}{\ln^2(z/z_0)} |u|^2$$

$$\tau_w = 0.5 \rho f_w u_b^2$$

- sediment dependant Z_0
- account of vertical elevation z which will vary in time and spatially

⇒ Bottom stress then is updated for sediment transport :

* For Bedload :
$$\theta_s = \frac{\tau_s}{(s-1)gd_{50}}$$

* For erosion/suspension :
$$Source = E_0 (1 - \varphi) \frac{\tau_b - \tau_{ce}}{\tau_{ce}}$$

Interfacing

* Waves input :

```
#define OW_COUPLING (WW3.nc...)  
#define WKB_WWAVE  
#define ANA_WWAVE
```

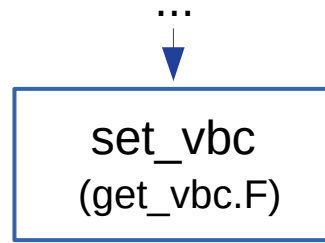
*Hs, Tp, DD,
(/ breaking
param/
Ub...)*

* Sediment inputs :

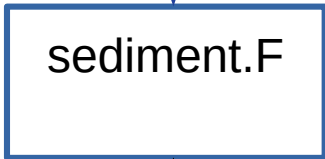
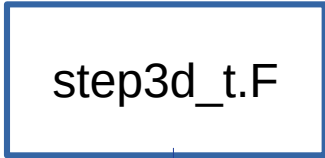
* by an input file (.nc)

* sediment.in :

```
→ #define ANA_SEDIMENT
```



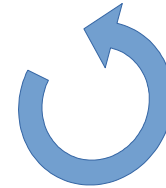
*Combined Wave/Current Bottom
stress : bostr / w(max) + Ripple
(Height/Length) + Zbapparent +
Ub*



*** Hydrodynamics + BBL +
waves + sediment routines**
(#define BBL)

Bedform roughness estimate at
the bottom (mean surface
properties) :

*Sdensity/Ssize/
taucb /settling
velocity*



* Update

3D bed properties (fraction / mass /
thickness ...)

2D bottom properties (Sdensity...)

Model options

BBL

Related CPP options:

BBL	Activate bottom boundary layer parametrization
ANA_WWAVE	Set analytical (constant) wave forcing (hs, Tp, Dir).
ANA_BSEDIM	Set analytical bed parameters (if SEDIMENT is undefined)
Z0_BL	Compute bedload roughness for ripple predictor and sediment purposes
Z0_RIP	Determine bedform roughness ripple height and ripple length for sandy bed
Z0_BIO	Determine (biogenic) bedform roughness ripple height and ripple length for silty beds

Preselected options:

```
#ifdef BBL
# ifdef OW_COUPLING
# elif defined WAVE_OFFLINE
# elif defined WKB_WWAVE
# else
# define ANA_WWAVE
# endif
# ifdef SEDIMENT
# undef ANA_BSEDIM
# else
# define ANA_BSEDIM
# endif
# ifdef SEDIMENT
# define Z0_BL
# else
# undef Z0_BL
# endif
# ifdef Z0_BL
# define Z0_RIP
# endif
# undef Z0_BIO
#endif
```

Morphodynamics

Exner equation : divergence of sediment fluxes

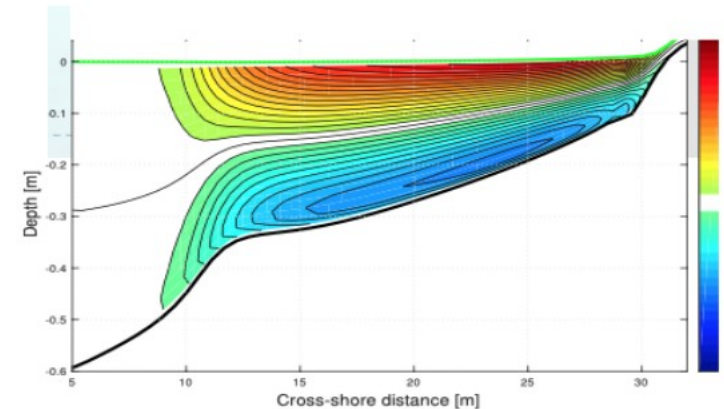
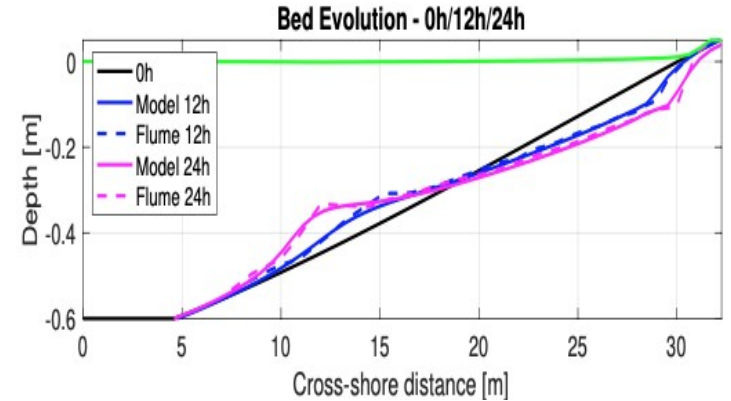
$$\frac{\partial z_b}{\partial t} = -\frac{f_{mor}}{1-p} \left(\frac{\partial q_b}{\partial x} - w_s \frac{\partial C}{\partial z} + E \right).$$

i.e. difference between erosion and deposition
+ bedload fluxes

- * modification of vertical velocity
- * acceleration of bed response
- * speed-up equilibration

- * change morphodynamics, change the dynamics, change the circulation , then move the bed

Ex Sandbar test case :



Interfacing

Runtime



bbl.F



...



step3d*.F



sediment.F

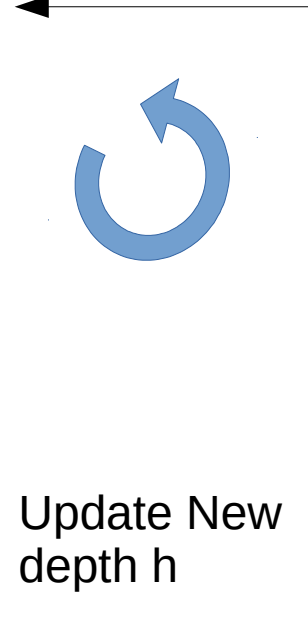


...

dh = total bed
thickness
differences

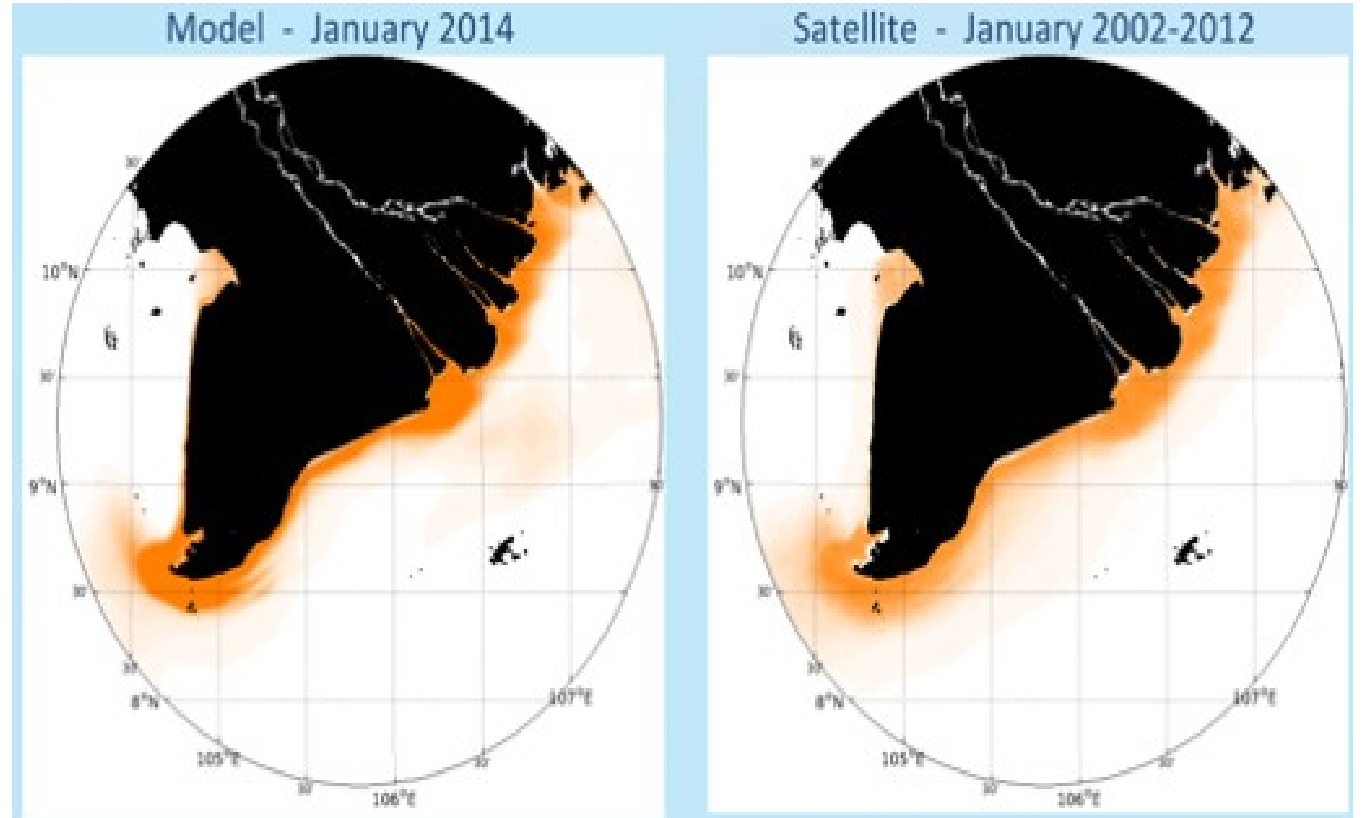
*** Hydrodynamics + BBL +
waves + Sediment routines
+ Morphodynamics**

set_depth



Update New
depth h

Examples 1



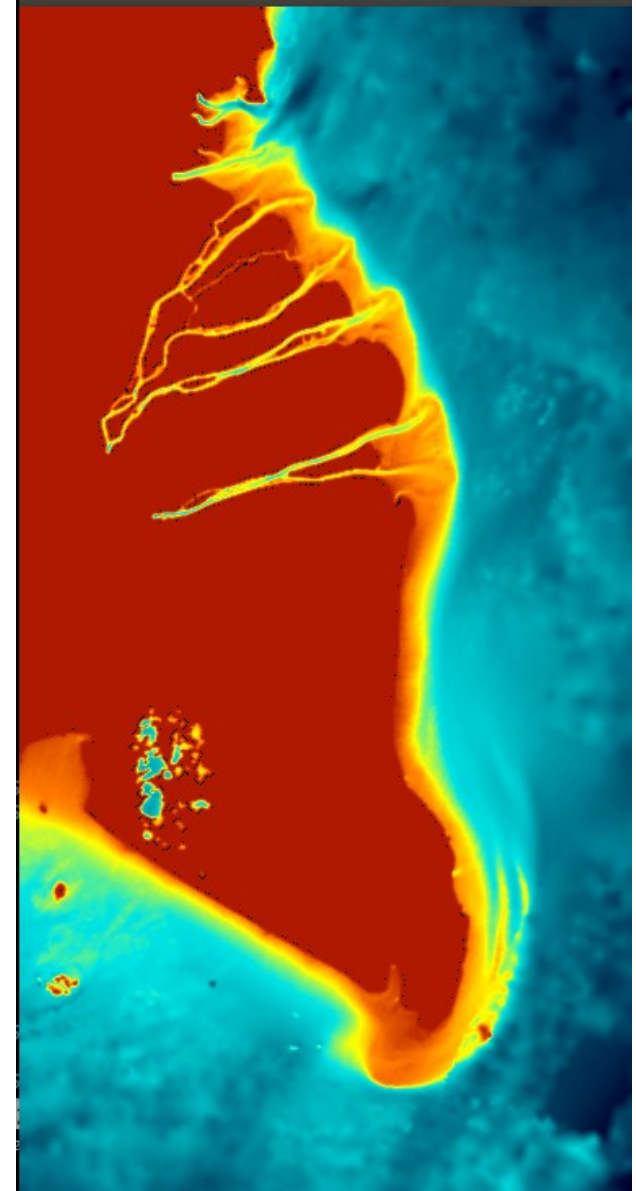
Gratiot et al., 2017, Ha et al., 2018, Marchesiello et al., 2019

- Example1 LMDCZ (Lower Mekong Delta Coastal Zone)

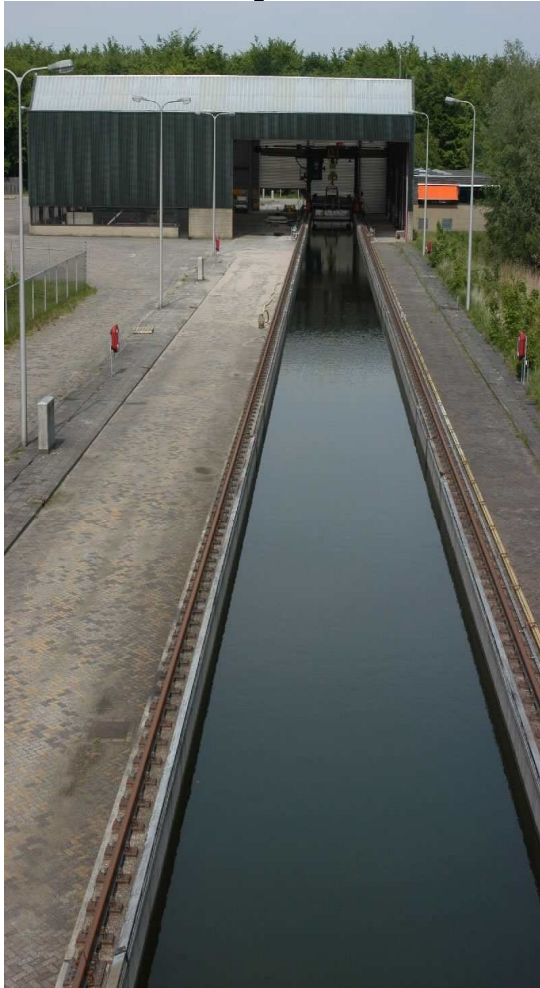
Resolution	550m	
Grid rectangular rotated grid Lx/Ly Lz	376/729 (374/727 calcul) 10	207/400 km 42,7m
bathy	SIWWR data + GEBCO	
RUNOFF	Clim from obs	1m
Tide	TPXO8 1/30°	
Oforc	ECCO	0,25° 3d
Aforc	ERA-interim	1° 6h
Wave	ERA-interim	1° 6h
Sediment (no cohesive behavior)	Sand) d50 200um Mud) d50 20um	Ws 20 mm/s Ws 0,03mm/s

Sand) d50 200um
Mud) d50 20um

2 classes of sediment

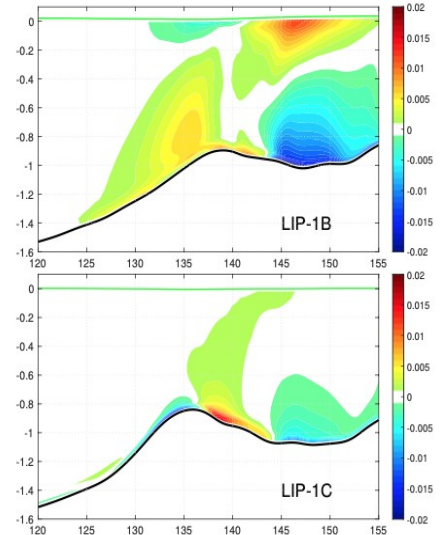
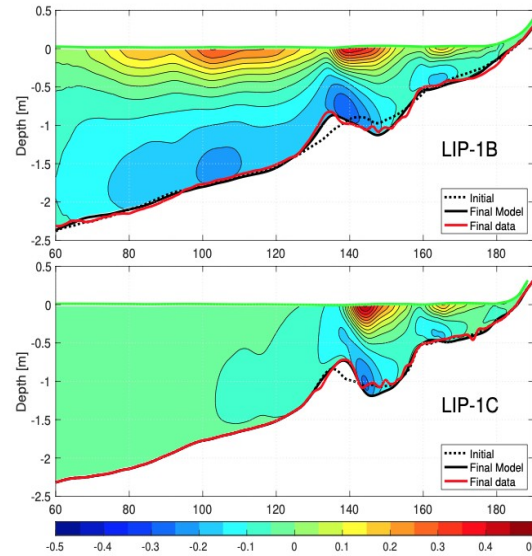
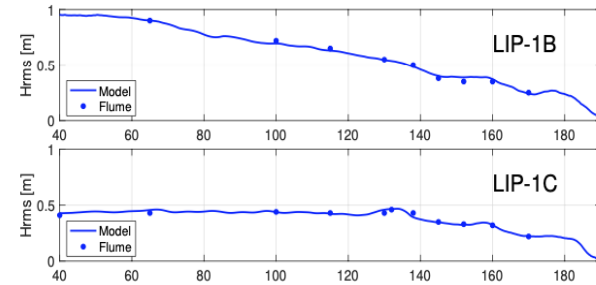


Examples 2



Erosion

Accretion



SUMMARY

Currently :

- * Increasing effort
- * Focus on sandy/wave dominated environment
- * More and more confident
- * Wave resolved configurations !

Underway :

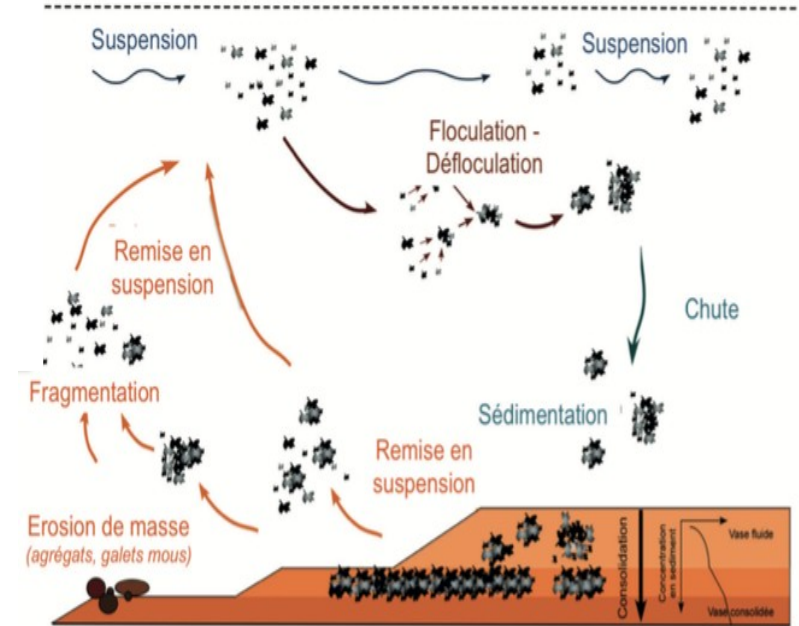
Consolidation / flocculation

TBD

interaction with vegetation

bio diffusion

Effect on density



BEDLOAD formula

Wu & Lin

* Added to compare with Mustang model

* Take account of hiding/exposure effects by using hidden and exposed probabilities of each sediment particle in the bed material

Transport rate
(class dependent) : $\Phi = \max [0, 0053 ((\theta_s - \tau_{ce}) / \tau_{ce})^{2,2} , 0]$

$$\theta_s = \frac{\tau_s}{(s - 1)gd_{50}} \quad \text{Shield parameter}$$

τ_{ce} Critical shear stress

τ_s : skin friction

Cppkey :
#defined BEDLOAD_WULIN