

CROCO

Coastal and Regional Ocean COmmunity model

USGS within Croco

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OUTLINE

- * USGS model presentation
- * Recap on sediment model and features
 - * Bedload formulas
 - * Suspended load
 - * Bed model
- * Implementation of USGS within CROCO :
 - * Equations
 - * Code structure
 - * Parameters and input files
 - * Possible interfaces
 - * Waves forcing
 - * Bottom Boundary Layer
 - * Morphodynamics
- * Examples

USGS Sediment model :

- * Activated with the cppkey « #define SEDIMENT »
- * « legacy » model within CROCO
- * Native one, from the UCLA/ROMS Community / USGS also called as CSTMS model (package Community Sediment Transport Modeling System), Blaas et al. (2007), Warner et al. (2008) and Shafiei et al. (2021)
- * Originally included in ROMS-AGRIF, some divergences appears with CROCO version but there are some common development
- * Available in ROMS-RUTGERS and OAWST

USGS

- Recap on sediment model and features

BEDLOAD formulas

Bedload flux :

$$q_b = \Phi \sqrt{(s - 1)gd_{50}^3 \rho_s}$$

d_{50} : median size

ρ_s : grain density

τ_c : critical stress

$$s = \rho / \rho_s$$



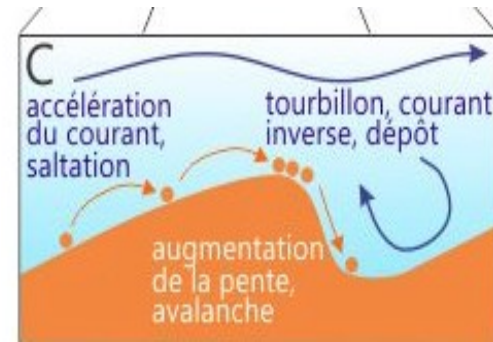
⇒ Different parameterization available for the transport rate Φ

Adding Slope effect :

$$q_b = q_b \left(\frac{0.65}{(0.65 - \tan \beta) \cos \beta} \right) \quad \beta = \tan^{-1}(dz_b/dx)$$

cppkey

#define LESSER (by default)



Cppkey :

#define BEDLOAD

Bedload : Meyer-Peter Müller (MPM) formulation

Case of rivers, continental shelves etc :

Transport rate
(class dependent) : $\Phi = \max [8(\theta_s - \theta_c)^{1.5}, 0]$

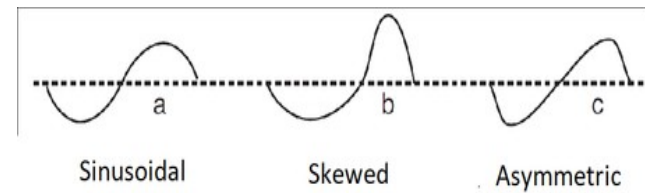
$$\theta_s = \frac{\tau_s}{(s-1)gd_{50}} \quad \text{Shield parameter}$$

θ_c : critical Shield parameter (0,047)

τ_s : skin friction

Cppkey :
#define BEDLOAD_MPM

Bedload : Vander A formulation



Case of non-linear waves : asymmetric transport, lag effect ... :

- * Compute wave asymmetry effect
- * Shield parameter at half cycles
- * Evaluate phase lag

Transport rate

(class dependent) : crest + trough

$$\Phi = \frac{1}{T} \left[\frac{\theta_c}{|\theta_c|^{1/2}} T_c \left(\Omega_{cc} + \frac{T_c}{2T_{cu}} \Omega_{tc} \right) + \frac{\theta_t}{|\theta_t|^{1/2}} T_t \left(\Omega_{tt} + \frac{T_t}{2T_{tu}} \Omega_{ct} \right) \right],$$

$$\Omega_i = \mathcal{F}(\text{Shield } Cr) = \max \left(11 (|\theta_i| - \theta_{cr})^{1.2}, 0 \right),$$

Cppkey :

```
#define BEDLOAD_VANDERA
```

Suspended transport

For each sediment class grain (non cohesive) :

Suspended sediment transport

$$\frac{\partial C}{\partial t} + \frac{\partial U_i C}{\partial x_i} = \frac{\partial}{\partial x_i} \left(K_H \frac{\partial C}{\partial x_{1,2}} + K_V \frac{\partial C}{\partial x_3} \right) + \text{Sources / Sinks}$$

Erosion rate (E0) / Settling velocity (Ws) / critical shear stress for erosion are user defined

Erosion formulation

$$\text{Source} = E_0 (1 - \varphi) \frac{\tau_b - \tau_{ce}}{\tau_{ce}} \quad \text{when } \tau_b > \tau_{ce}$$

Bottom shear stress vs critical shear stress for erosion

If positive : material are added to the water column

Deposition formulation

$$\text{Sink} = w_s \frac{\partial C}{\partial z}$$

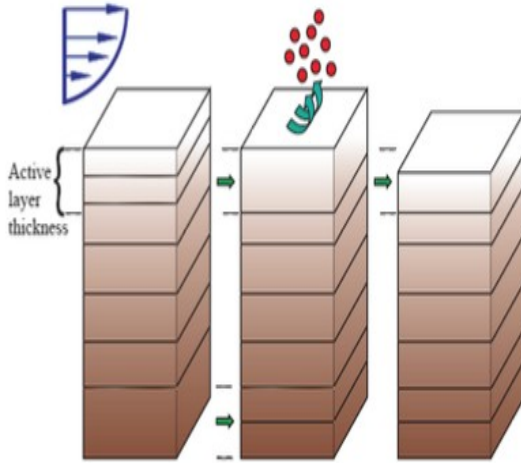
Settling velocity vs tracers gradient

Cppkey : #define SUSPLOAD

Bed model

Active layer thickness (Harris and Wiberg, 1997).

$$Z_a = k_1(\tau_w \cdot \tau_c) + k_2 D_{50}$$



Erosion. ($\tau_b > \tau_c$)

Mix sediment from lower layers so that surface layer is at least z_a thick. Split bottom layer. Erode from surface layer.

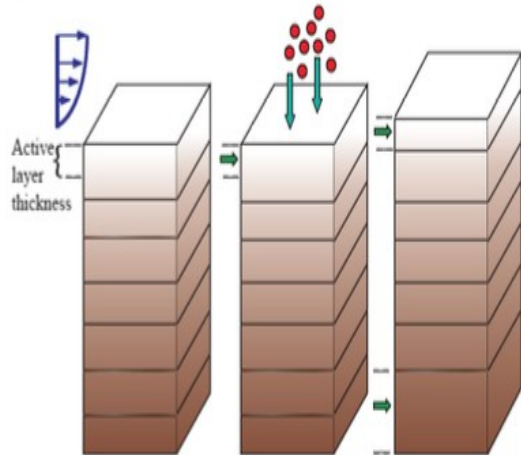
erosion_flux_i =

$$\text{MIN} \left[\begin{array}{l} dt \cdot E_i \cdot (1 - \text{poro}) \cdot \text{frac}_i \cdot (\tau_w / \tau_{c,i} \cdot 1) \\ \rho_i \cdot (1 - \text{poro}) \cdot \text{frac}_i \cdot z_a + \text{dep_flux}_i \end{array} \right]$$

Erosion

for $\tau_b > \tau_{ce}$

Number of layers is fixed



Deposition.

Rule: create new layer if deposition > 5 mm (user defined). Mix surface layer to be at least z_a thick. Combine bottom layer.

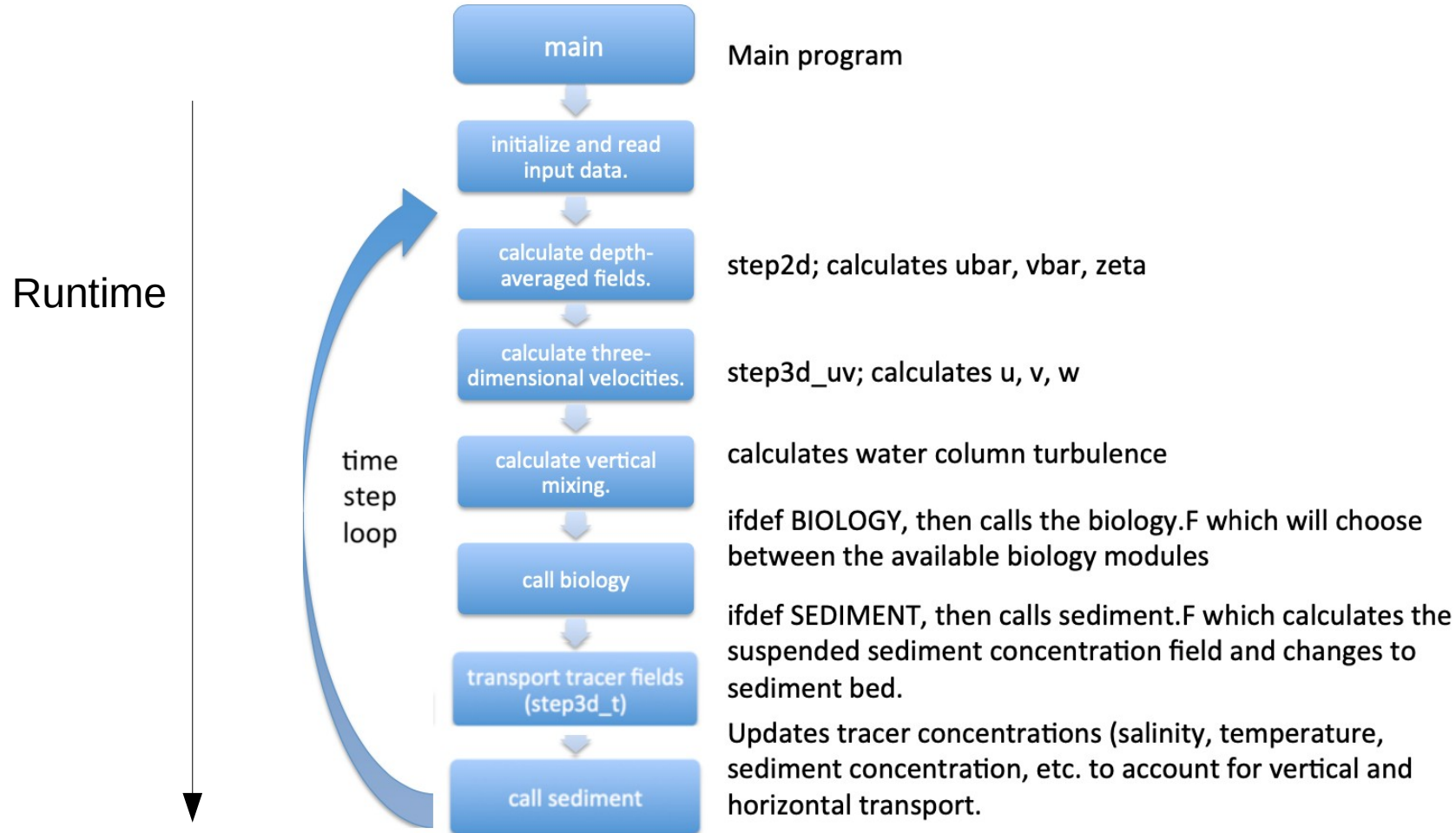
$$\frac{\partial C_i}{\partial t} = -w_{s,i} \frac{\partial C}{\partial z}$$

Deposition

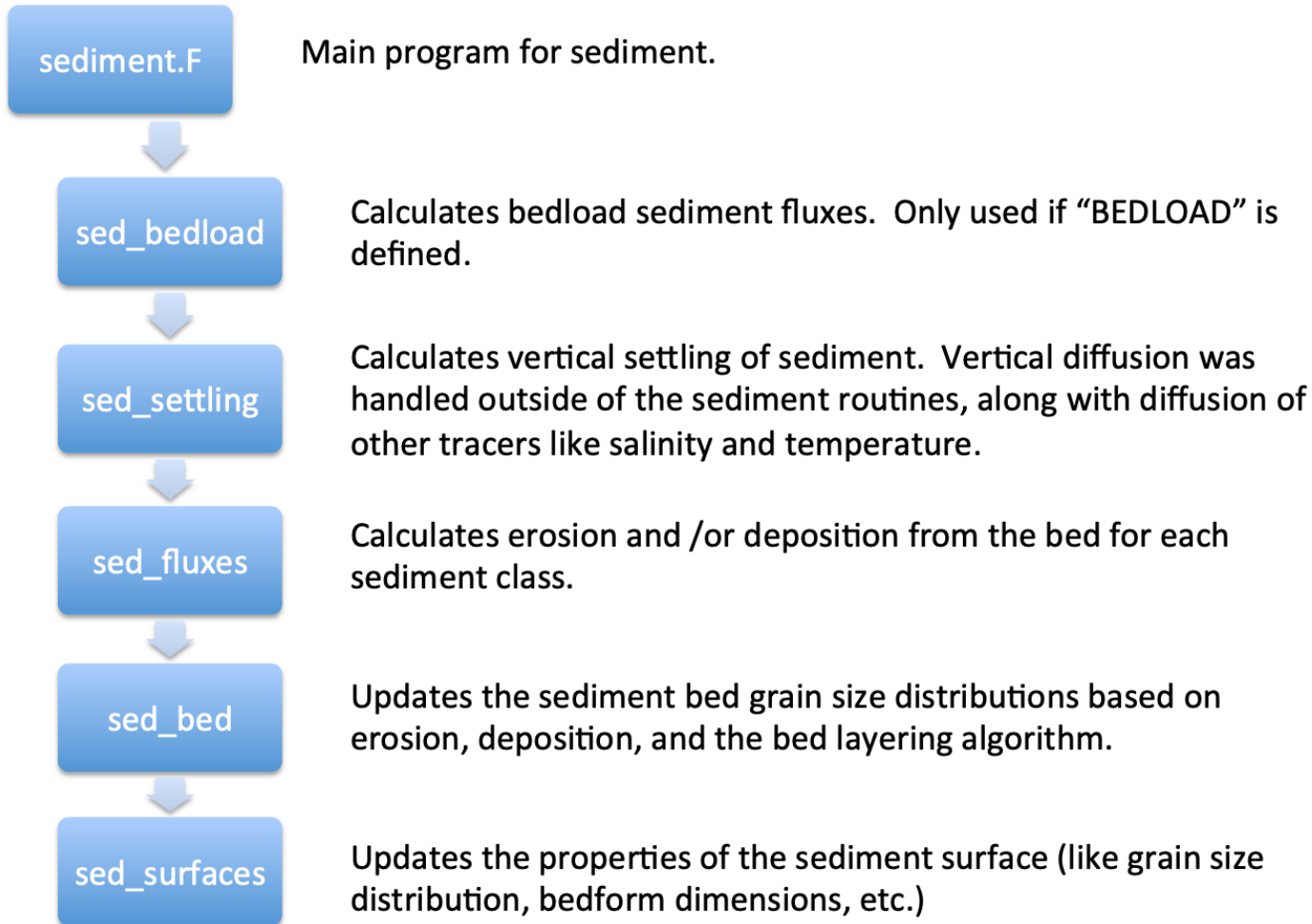
Rule: create a new layer for deposition if top layer > 1mm

Code structure

Code structure (1)



Code structure (2)



Model options

Sediment parameters

- Hard coded
 - Number of layers
 - Number of sediment classes

=> in param.h

```
!
# ifdef SEDIMENT
! NSAND      Number of sand classes
! NMUD       Number of mud classes
! NGRAV      Number of gravel classes (not implemented...)
! NST        Number of sediment (tracer) size classes
! NLAY       Number of layers in sediment bed
!
      integer NSAND, NMUD, NGRAV, NST, NLAY
# ifdef DUNE
#   ifdef ANA_DUNE
      parameter (NSAND=1, NMUD=0, NGRAV=0)
      parameter (NLAY=11)
#   else
      parameter (NSAND=2, NMUD=0, NGRAV=0)
      parameter (NLAY=10)
#   endif
# elif defined SED_TOY
#   if defined SED_TOY_RESUSP || defined SED_TOY_CONSOLID
      parameter (NSAND=2, NMUD=2, NGRAV=0)
      parameter (NLAY=41)
#   elif defined SED_TOY_FLOC
      parameter (NSAND=4, NMUD=15, NGRAV=0)
      parameter (NLAY=20)
#   elif defined SED_TOY_ROUSE
      parameter (NSAND=0, NMUD=6, NGRAV=0)
      parameter (NLAY=1)
#   endif
# else
      parameter (NSAND=2, NMUD=0, NGRAV=0)
      parameter (NLAY=1)
# endif
      parameter (NST=NSAND+NMUD+NGRAV)
      parameter (ntrc_sed=NST)
# else
      parameter (ntrc_sed=0)
# endif /* SEDIMENT */
!
```

Model options

Sediment CPP keys

- Main keys :
 - SEDIMENT
 - SUSPLOAD
 - BEDLOAD

=> stick with default choices

Related CPP options:

SUSPLOAD	Activate suspended load transport
BEDLOAD	Activate bedload transport
MORPHODYN	Activate morphodynamics
BEDLOAD_VANDERA	van der A formulation for bedload (van der A et al., 2013)
BEDLOAD_MPM	Meyer-Peter-Muller formulation for bedload (Meyer-Peter and Muller, 1948)
SLOPE_LESSER	Lesser formulation for avalanching (Lesser et al, 2004)
SLOPE_NEMETH	Nemeth formulation for avalanching (Nemeth et al, 2006)
BEDLOAD_UP1	Bedload flux interpolation: upwind 1st order
BEDLOAD_UP5	Bedload flux interpolation: upwind 5th order
BEDLOAD_WENO5	Bedload flux interpolation: WENO 5th order
ANA_SEDIMENT	Set analytical sediment size, initial ripple and bed parameters
ANA_BPFLUX	Set kinematic bottom flux of sediment tracer (if different from 0)
SPONGE_SED	Gradually reduce erosion/deposition near open boundaries

Preselected options:

```
#ifdef SEDIMENT
# undef MUSTANG
# define ANA_SEDIMENT
# define SPONGE_SED
# define Z0_BL
# define Z0_RIP
# ifdef BEDLOAD
#   ifdef BEDLOAD_VANDERA      /* default BEDLOAD scheme */
#   elif defined BEDLOAD_MPM
#   elif defined BEDLOAD_WULIN
#   elif defined BEDLOAD_MARIEU
#   else
#     if (defined WAVE_OFFLINE || defined WKB_WWAVE ||\
        defined ANA_WWAVE || defined OW_COUPLING)
#       define BEDLOAD_VANDERA
#     else
#       define BEDLOAD_MPM
#     endif
#   endif
# endif
```

Model options

Input file

- Dans croco.in :

```
sediments: input file
           sediment.in
sediment_history_fields: bed_thick bed_poros bed_fra(sand,silt)
                       20*F
```

- Additional file at run time : [sediment.in](#)

Consistent with param.h :

- Number of layers
- Number of sediment classes

```
1 Stitle (a80)
CROCO - Sediment - Test
2 Sd(1-NST), CSED, SRHO, WSED, ERATE, TAU_CE, TAU_CD, BED_FRAC(1:NLAY)
  0.125  9.9  2650.  9.4  25.0e-5  0.05  0.14  0.4  0.4
  0.050  0.0  2650.  1.6  4.0e-5  0.01  0.14  0.6  0.6
3 BTHK(1:NLAY)
  1.  10.
4 BPOR(1:NLAY)
  0.41  0.42
5 Hrip
  0.03
6 Lrip
  0.14
7 bedload_coeff
  0.
8 morph_fac
  10.
99 END of sediment input data
```

> **Sd** : Diameter of grain size class [mm].

> **CSED** : Initial concentration (spatially uniform) [kg/m³].

> **SRHO** : Density of sediment material of size class [kg/m³].

Quartz: SRHO=2650 kg/m³

> **WSED** : Settling velocity of size class [mm/s].

Typically (Soulsby, 1997):

$$WSED = 10^3 (visc (\sqrt{10.36^2 + 1.049D^3} - 10.36) / D_{50} \text{ [mm/s]})$$

$$\text{with } D = D_{50} (g (SRHO/\rho_0 - 1) / (visc^2))^{0.33333}$$

$$D_{50} = 10^{-3} Sd \text{ [m]}$$

$$visc = 1.3 \cdot 10^{-3} / \rho_0 \text{ [m}^2/\text{s]}$$

> **ERATE** : Erosion rate of size class [kg/m²/s].

Typically:

$$ERATE = 10^{-3} \gamma_0 WSED SRHO \text{ [kg/m}^2/\text{s]}$$

$$\text{with } \gamma_0 = 10^{-3} - 10^{-5} \text{ (Smith \& McLean, 1977)}$$

> **TAU_CE** : Critical shear stress for sediment motion [N/m²]

(initiation of bedload for coarses, suspension for fines). Typically : $TAU_{CE} = 6.4 \cdot 10^{-7} \rho_0 WSED^2$ [N/m²]

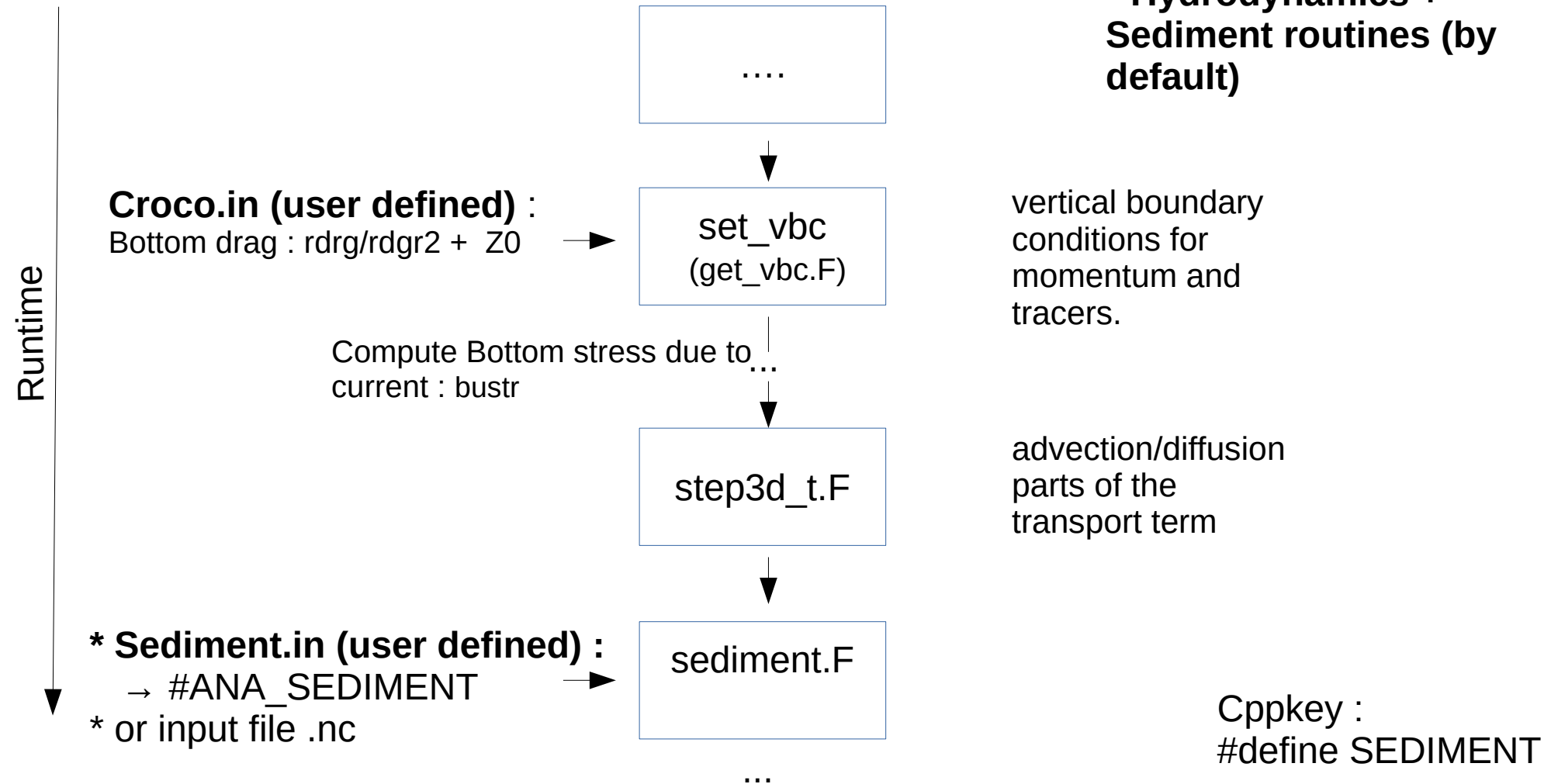
> **TAU_CD** : Critical shear stress for deposition of cohesive sediments [N/m²]

> **BED_FRAC** : Volume fraction of each size class in each bed layer (NLAY columns)

$$[0 < BED_FRAC < 1]$$

Possible interfacing

No Interfacing



Waves forcing overview

Description	Analytical Specified / constant value	Internal Wave Maker Waves resolving simulation (Non boussinesq / w solve explicetely)	Embedded wave model within Croco		Online data	Offline data
			WKB primary waves and empirical breaking model parameters with offshore wave amplitud/period boundary conditions		Spectral wave model (WW3..)	clim/reanalysis (ERA5...)
			Initialized by croco.in	boundary forcing from other wave data		
Advantages	Cheap	better resolved at the bottom / no use of wave average equation	Cheap / No waves generation / parametrizations for wave breaking and bottom drag		Realistic	
cppkey	#ANA_WWAVE	#WAVE_MAKER #NBQ	#WKB_WWAVE #ANA_BRY_WKB	#WKB_WWAVE	#OW_COUPLING	#WAVE_OFFLINE
routine	analytical.F	wave_maker*.h	wkb_wwave.F		get_wwave.F	
				get_bry_wkb.F		
Parameters	Hs,T,DD	Hs,T,DD...	Hs, T, DD + breaking parameters			
User def. file	Analytical.F	wave_maker*.h	Croco.in (wkb_wwave/wkb_roller)			

⇒ Estimate wave associated variables usually pass to wave current interaction (#MRL_WCI) (based on wave average equation, compute additional terms , stokes drift) and Bottom Boundary layer (#BBL) routines

Bottom boundary layer

Goal :

- * Variability of gradients in velocity and suspended-sediment concentrations near the bottom
- * Take account of the change of rugosity due to sediment in bottom stress computation
- * Parameterize the effect of surface waves on bottom stresses and apparent roughness

⇒ **BBL formulation :**

$$\bar{\tau}_{wc} = \tau_c \left(1 + 1.2 \left(\frac{\tau_w}{\tau_w + \tau_c} \right)^{3.2} \right)$$

- account for current stress at the bottom
- account for wave stress

$$\tau_c = \frac{\kappa^2}{\ln^2(z/z_0)} |u|^2$$

$$\tau_w = 0.5 \rho f_w u_b^2$$

- sediment dependant Z_0
- account of vertical elevation z which will vary in time and spatially

⇒ Bottom stress then is updated for sediment transport :

* For Bedload :
$$\theta_s = \frac{\tau_s}{(s-1)gd_{50}}$$

* For erosion/suspension :
$$Source = E_0 (1 - \varphi) \frac{\tau_b - \tau_{ce}}{\tau_{ce}}$$

Interfacing

* Waves input :

```
#define OW_COUPLING (WW3.nc...)  
#define WKB_WWAVE  
#define ANA_WWAVE
```

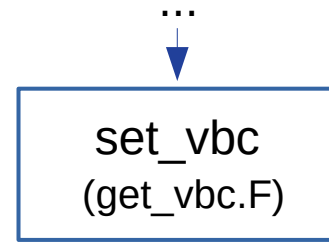
*Hs, Tp, DD,
(/ breaking
param/
Ub...)*

* Sediment inputs :

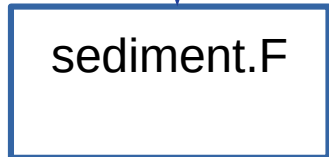
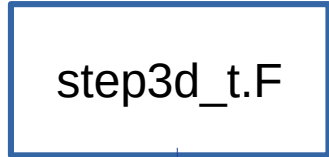
* by an input file (.nc)

* sediment.in :

→ #define ANA_SEDIMENT



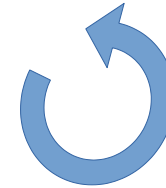
*Combined Wave/Current Bottom
stress : bostr / w(max) + Ripple
(Height/Length) + Zbapparent +
Ub*



*** Hydrodynamics + BBL +
waves + sediment routines**
(#define BBL)

Bedform roughness estimate at
the bottom (mean surface
properties) :

*Sdensity/Ssize/
taucb /settling
velocity*



* Update

3D bed properties (fraction / mass /
thickness ...)

2D bottom properties (Sdensity...)

Model options

BBL

Related CPP options:

BBL	Activate bottom boundary layer parametrization
ANA_WWAVE	Set analytical (constant) wave forcing (hs, Tp, Dir).
ANA_BSEDIM	Set analytical bed parameters (if SEDIMENT is undefined)
Z0_BL	Compute bedload roughness for ripple predictor and sediment purposes
Z0_RIP	Determine bedform roughness ripple height and ripple length for sandy bed
Z0_BIO	Determine (biogenic) bedform roughness ripple height and ripple length for silty beds

Preselected options:

```
#ifdef BBL
# ifdef OW_COUPLING
# elif defined WAVE_OFFLINE
# elif defined WKB_WWAVE
# else
# define ANA_WWAVE
# endif
# ifdef SEDIMENT
# undef ANA_BSEDIM
# else
# define ANA_BSEDIM
# endif
# ifdef SEDIMENT
# define Z0_BL
# else
# undef Z0_BL
# endif
# ifdef Z0_BL
# define Z0_RIP
# endif
# undef Z0_BIO
#endif
```

Morphodynamics

Exner equation : divergence of sediment fluxes

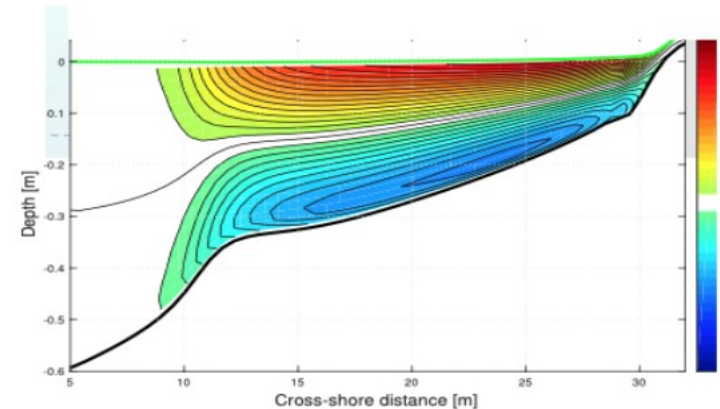
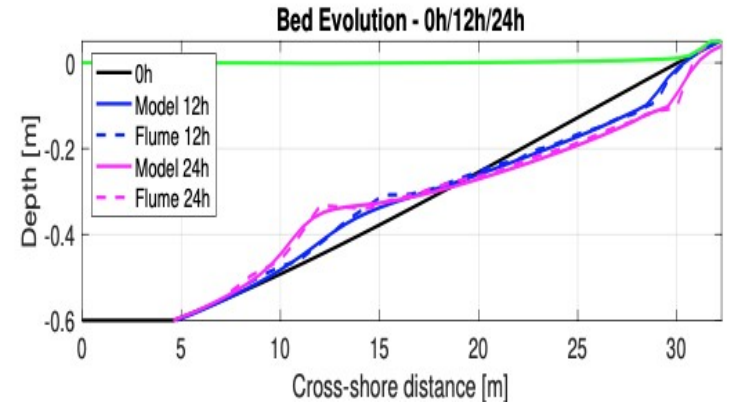
$$\frac{\partial z_b}{\partial t} = -\frac{f_{mor}}{1-p} \left(\frac{\partial q_b}{\partial x} - w_s \frac{\partial C}{\partial z} + E \right).$$

i.e. difference between erosion and deposition
+ bedload fluxes

- * modification of vertical velocity
- * acceleration of bed response
- * speed-up equilibration

- * change morphodynamics, change the dynamics, change the circulation , then move the bed

Ex Sandbar test case :



Interfacing

Runtime



bbl.F



...



step3d*.F



sediment.F

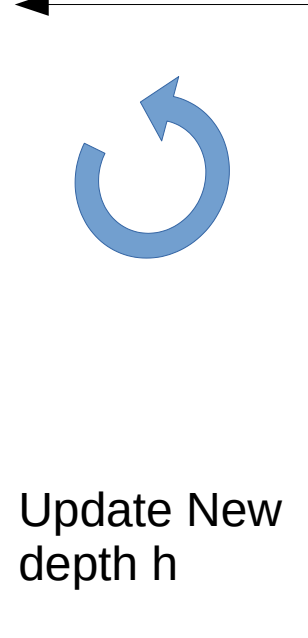


...

dh = total bed
thickness
differences

*** Hydrodynamics + BBL +
waves + Sediment routines
+ Morphodynamics**

set_depth



Update New
depth h

Sandbar

Goal :

To predict onshore and offshore sandbar migrations under storm and post-storm conditions

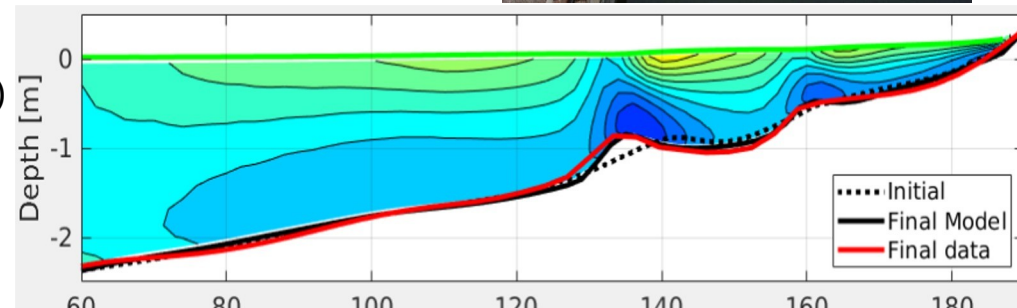
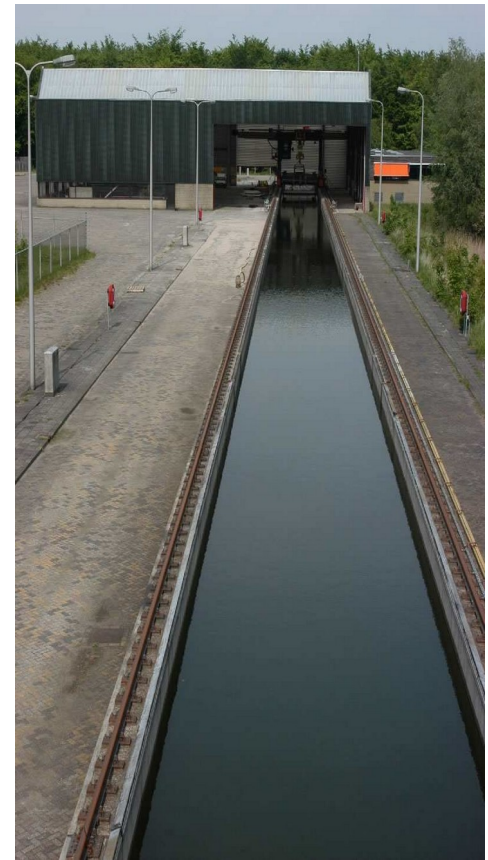
To Fit well with sandbar experiment data from European Large Installation Plan (LIP) :

- * LIP-1B (characterizing erosion of sandbar) **SANDBAR_OFFSHORE**
- * LIP-1C (accretion) **SANDBAR_ONSHORE**

Different Wave Forcing methods :

* Wave statistics from WKB wave model that will initialize a Bottom Boundary Layer and Use of wave current interactions

* Use of Wave maker for wave-resolving simulations in Non hydrostatic mode (NBQ) (need high resolution at the bottom)



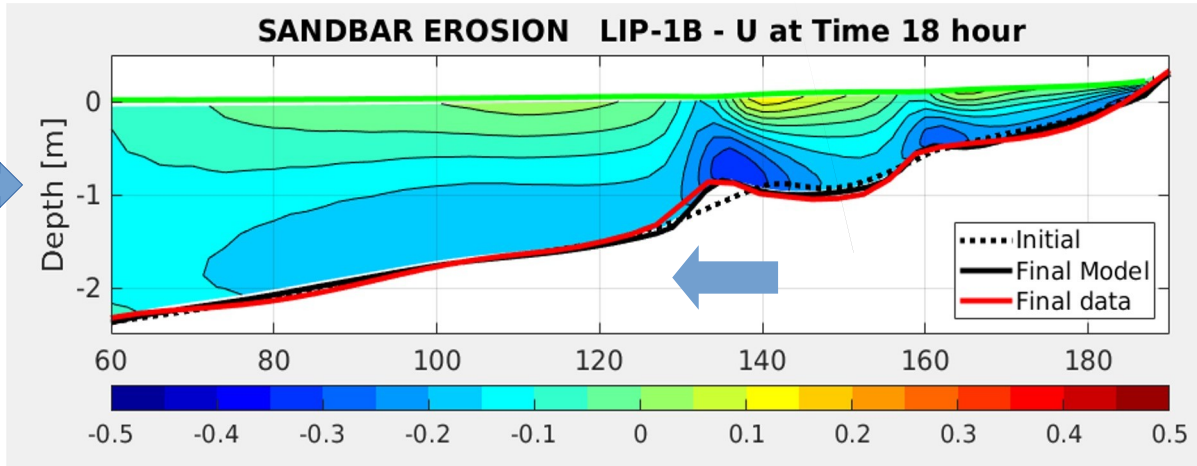
t_0

Initialize beach profile with linear slope

Dean number $De = H_s / T_p W_s$
(Erosion vs Accretion)
 $W_s = 25 \text{ mm/s}$

t_1

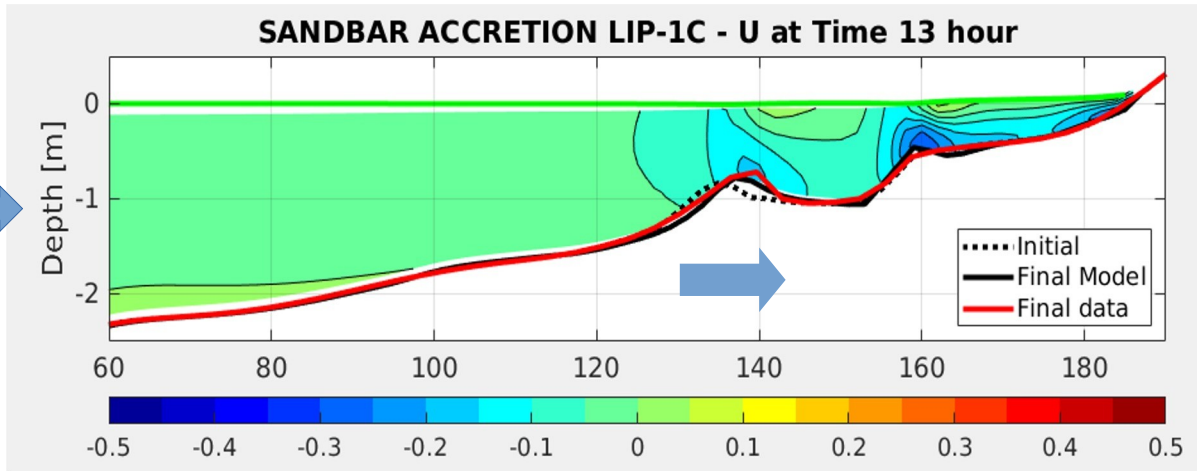
High energy waves :
 $H_s = 0,45 \text{ m}$
 $T_p = 5 \text{ s}$



$De = 3,6$
 \Rightarrow **Erosion**

$t_2 = t_1 + 18 \text{ h}$

Low energy waves :
 $H_s = 0,18 \text{ m}$
 $T_p = 8 \text{ s}$



$De = 0,9$
 \Rightarrow **Accretion**

$t_2 + 13 \text{ h}$

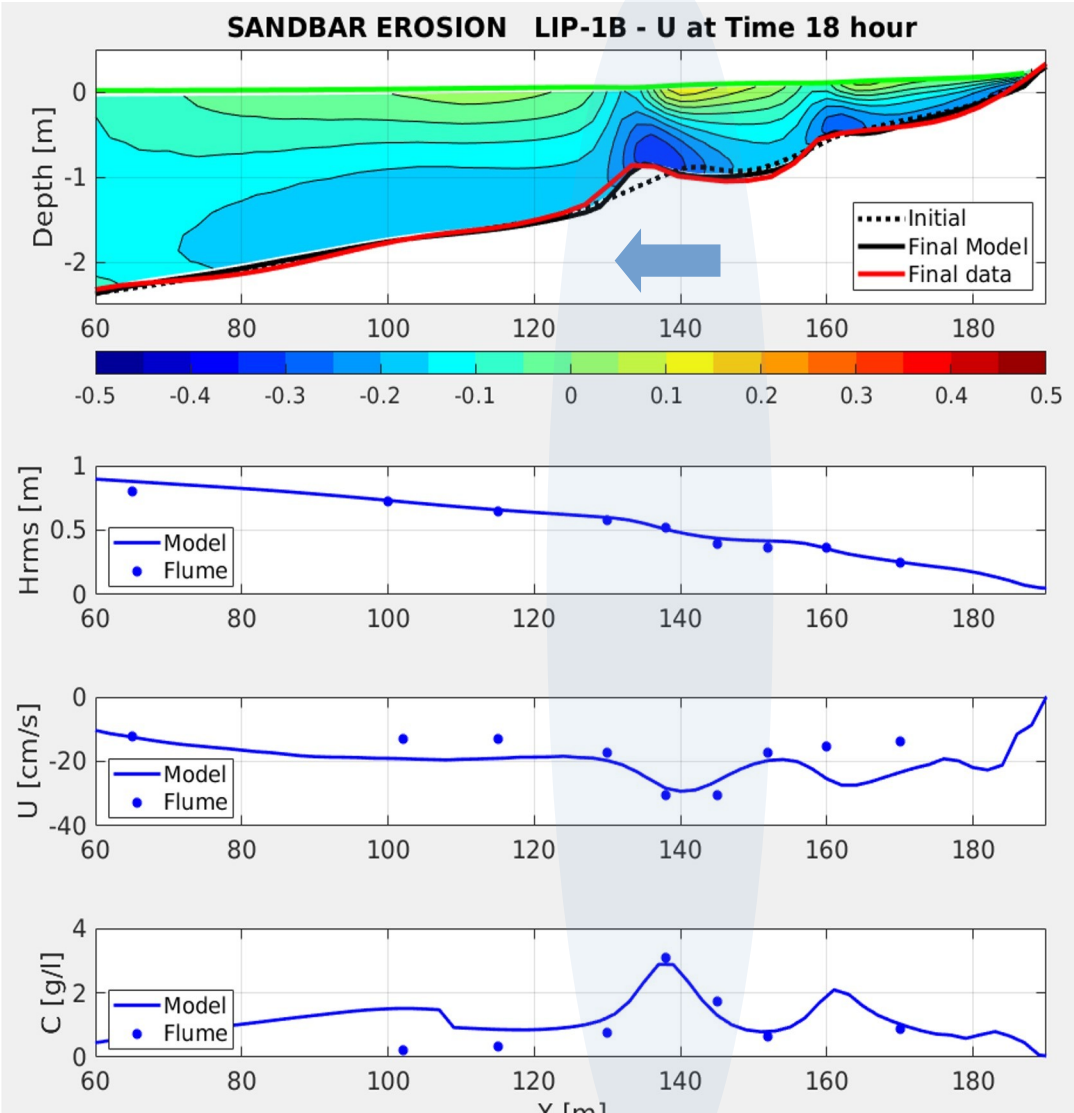
Validation with LIP-1B flume experiment

* Transport increase onshore to offshore

* Hrms : root-mean-square wave height (fit well with flume data)

* Undertow

* Bottom Concentration is correlated with undertow
Resuspended material greater



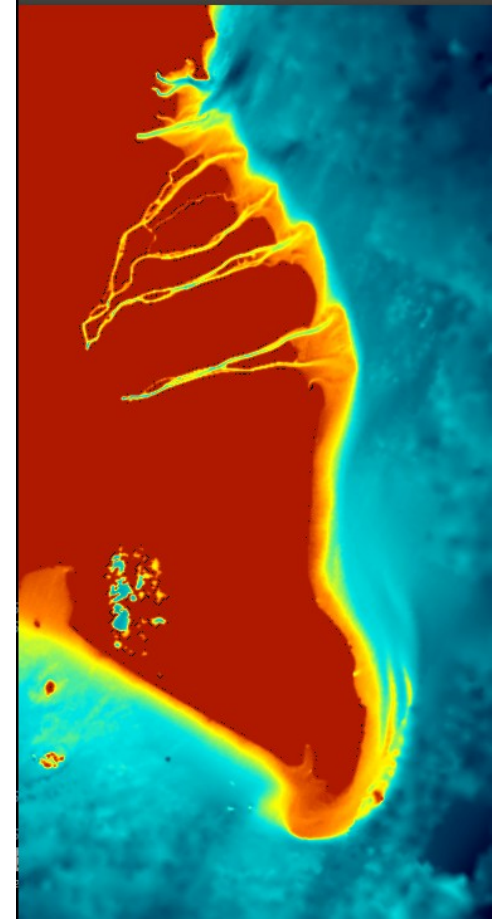
Examples 1

* Study of accretion / erosion processes due to interaction between Mekong river / tides / waves

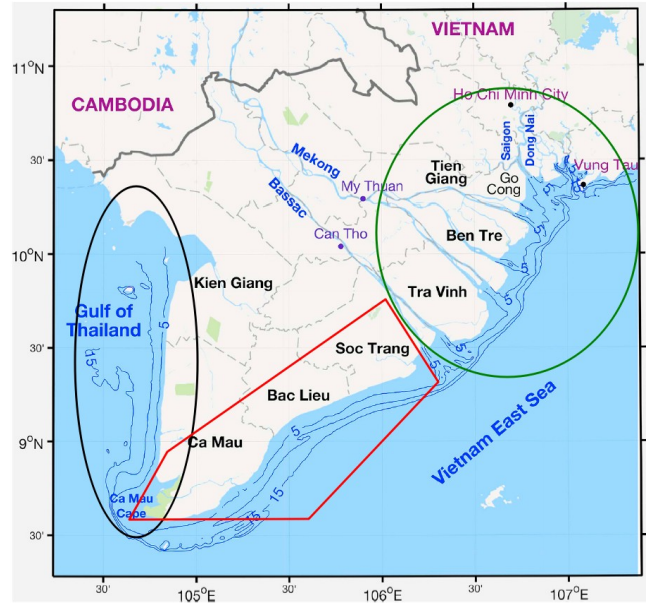
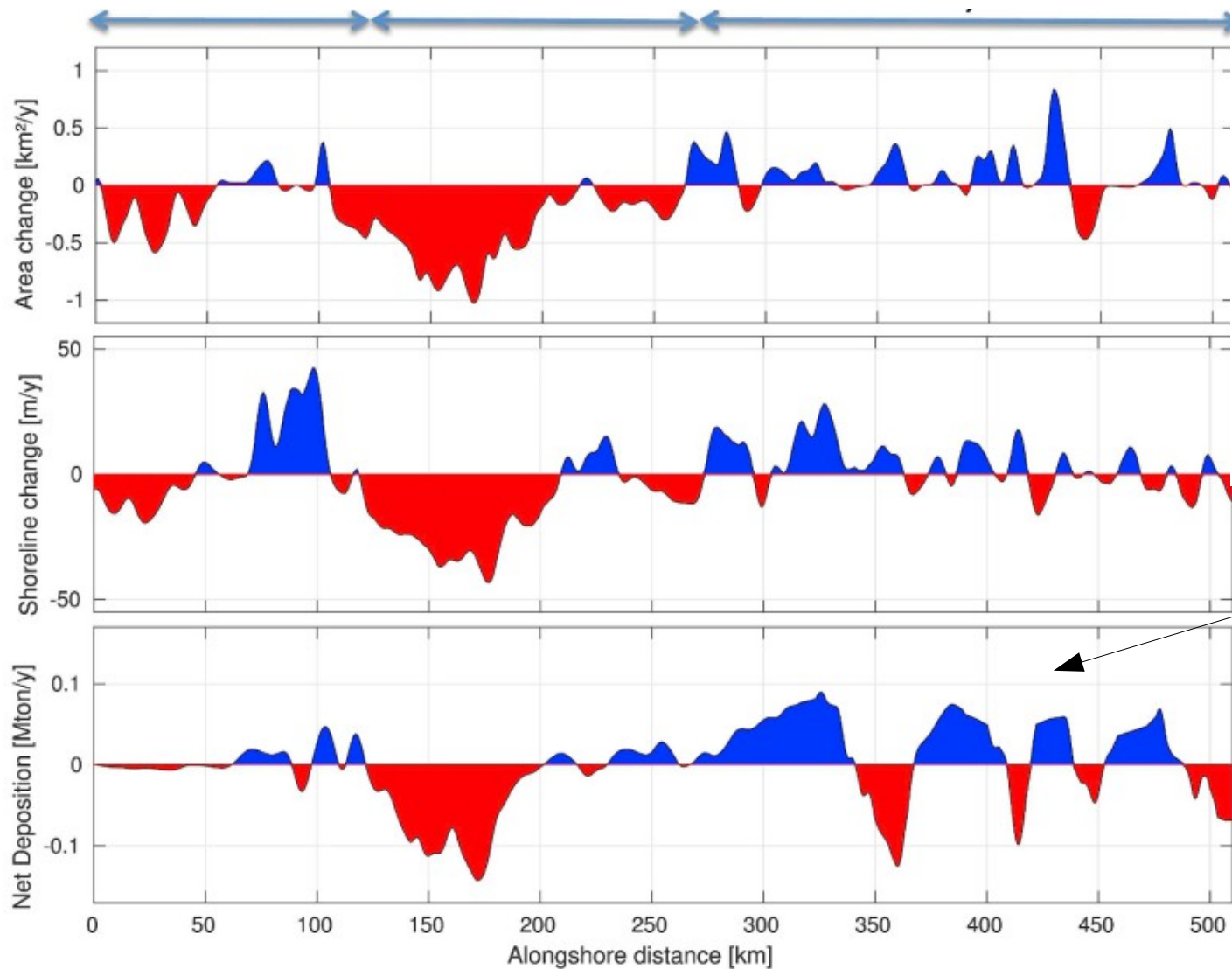
→ Configuration Croco **LMDCZ** (Updated version):

Resolution	550m	
Grid rectangular rotated grid Lx/Ly Lz	376/729 (374/727 calcul) 10	207/400 km 42,7m
bathy	SIWWR data + GEBCO	
RUNOFF	Clim from obs (2017-2019)	1m
Tide	TPXO9 v5 (1/30°)	
Oforc	Reanalysis GLORYS (1/12)	0,25° 1d
Aforc	ERA5	0.25° 1h
Wave	ERA5	0.5° 1h
Sediment (no cohesive behavior)	Sand) d50 200um Mud) d50 20um	Ws 20 mm/s Ws 0,03mm/s

2 classes of sediment



WEST COAST EAST COAST ESTUARY ZONE



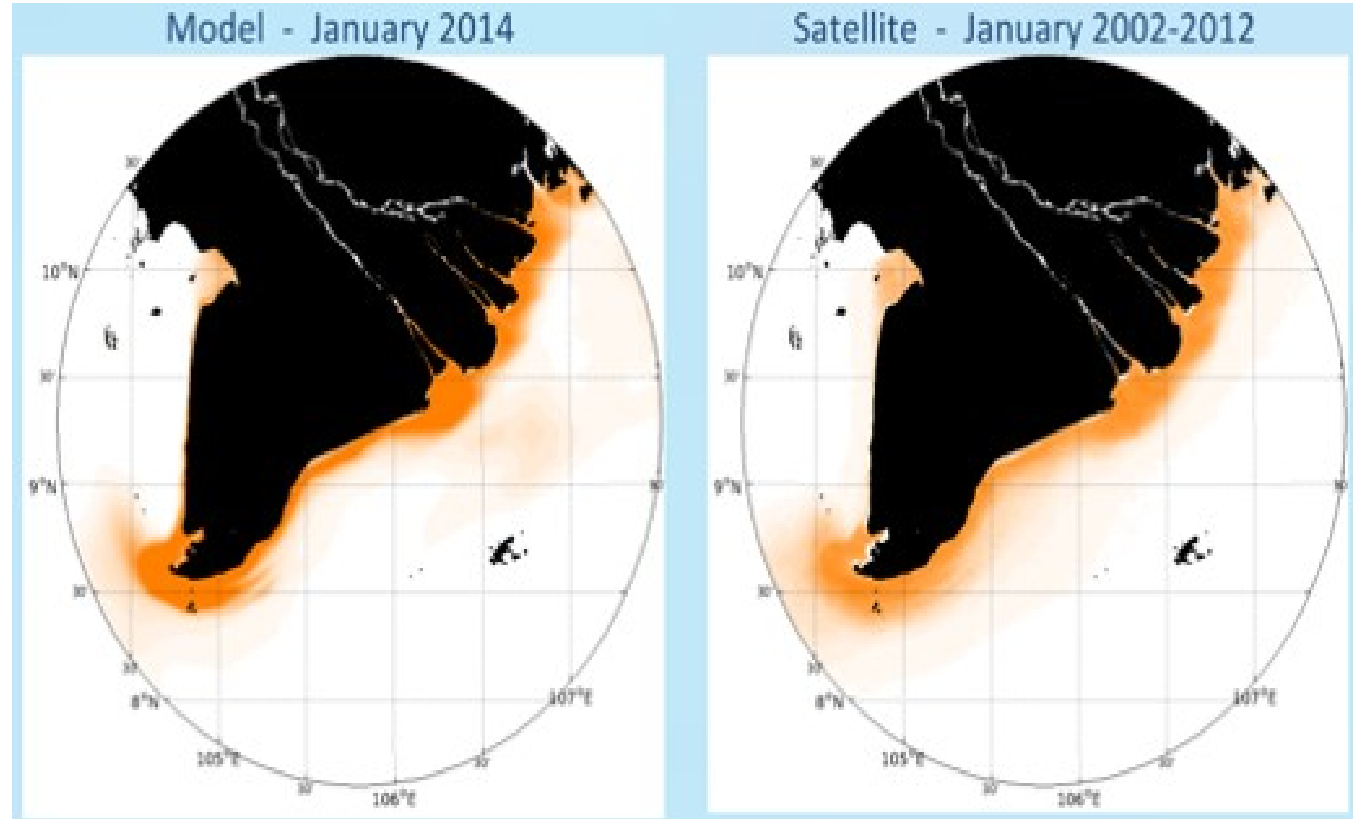
Model net deposition
along the whole
Mekong delta coastline

Accretion

Erosion

Validation :

Product of satellite MERIS (surface particulate matter)



Gratiot et al., 2017, Ha et al., 2018, Marchesiello et al., 2019

